

OPAx863A High-Precision, 105-MHz, Rail-to-Rail Input and Output Amplifier

1 Features

- Gain-bandwidth product: 50-MHz
- High precision
 - Input offset voltage: 95- μ V (maximum)
 - Offset drift: 1.2- μ V/°C (maximum)
- Low power
 - Quiescent current: 800- μ A/ch (typical)
 - Supply voltage: 2.7-V to 12.6-V
- Input voltage noise: 6.3-nV/ $\sqrt{\text{Hz}}$
- Slew rate: 100-V/ μ s
- Rail-to-rail input and output
- HD₂/HD₃: –129 dBc/–138 dBc at 20 kHz (2-V_{PP})
- Operating temperature range: –40°C to +125°C
- Additional features:
 - Overload power limit
 - Output short-circuit protection

2 Applications

- Low-power SAR and $\Delta\Sigma$ ADC driver
- ADC reference buffer
- Low-side current sensing
- Photodiode TIA interface
- Inductive sensing
- Battery-powered instrumentation
- Gain and active filter stages

3 Description

The OPAx863A devices are low-power, unity-gain stable, rail-to-rail input and output, voltage-feedback operational amplifiers, trimmed in package to offer high precision performance with maximum input offset voltage of 95- μ V and offset drift of 1.2- μ V/°C for high accuracy measurements over temperature.

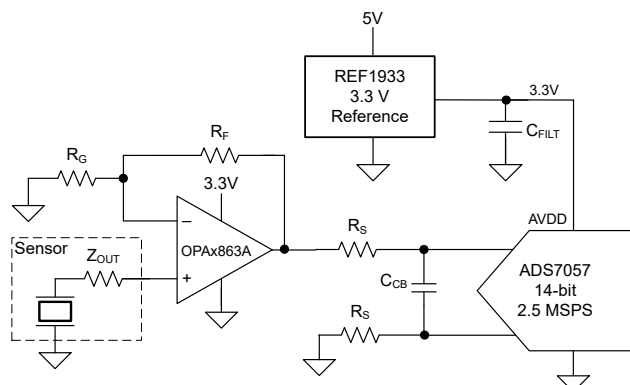
Consuming only 800- μ A per channel, the OPAx863A devices offer a gain-bandwidth product of 50-MHz, slew rate of 100-V/ μ s with a voltage noise density of 6.3-nV/ $\sqrt{\text{Hz}}$. The rail-to-rail input stage with 2.7-V supply operation is useful in portable battery powered applications. The rail-to-rail input stage is well matched for gain-bandwidth product and noise across the full input common-mode voltage range, enabling superior performance with wide-input dynamic range.

The OPAx863A devices include overload power limiting to limit the increase in I_Q with saturated outputs, thereby preventing excessive power dissipation in power conscious battery-operated systems. The output stage is short-circuit protected, making it conducive to ruggedized environments.

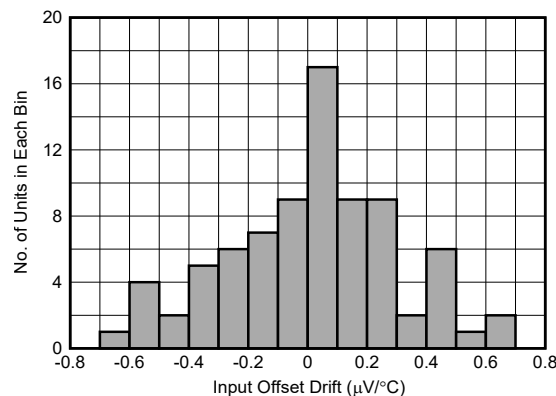
Package Information⁽¹⁾⁽³⁾

PART NUMBER	PACKAGE	BODY SIZE (NOM)
OPA863A	DBV (SOT23, 5) ⁽²⁾	2.90 mm × 1.60 mm
OPA2863A	DSN (USON, 10)	3.00 mm × 3.00 mm

- For all available packages, see the orderable addendum at the end of the data sheet.
- Preview packages.
- See the [Device Comparison Table](#)



OPAx863A as Precision SAR ADC Input Driver



Precision Performance with Low Input Offset Voltage Drift



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4 Revision History

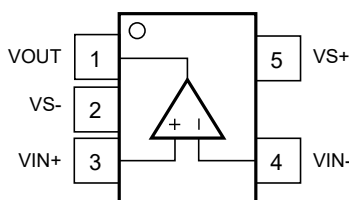
NOTE: Page numbers for previous revisions may differ from page numbers in the current version.

Changes from Revision A (December 2022) to Revision B (December 2022)	Page
• Changed the description for the $\overline{\text{PD1}}$ and $\overline{\text{PD2}}$ pins from: <i>high/floating = enabled</i> to: <i>high = enabled</i>	3
Changes from Revision * (May 2022) to Revision A (December 2022)	Page
• Changed the status of the data sheet from: <i>Advanced Information</i> to: <i>Production Data</i>	1

5 Device Comparison Table

DEVICE	$\pm V_S$ (V)	I_Q / CHANNEL (mA)	GBWP (MHz)	SLEW RATE (V/ μ s)	VOLTAGE NOISE (nV/ $\sqrt{\text{Hz}}$)	AMPLIFIER DESCRIPTION
OPAx863A	± 6.3	0.80	50	100	6.3	Unity-gain stable RRIO Bipolar Amplifier
LMH6643	± 6.4	2.7	65	130	17	Unity-gain stable NRI/RRIO Bipolar Amplifier
OPAx810	± 13.5	3.6	70	200	6.3	Unity-gain stable RRIO FET-Input Amplifier
OPAx837	± 2.7	0.6	50	105	4.7	Unity-gain stable NRI/RRIO Bipolar Amplifier
OPAx607	± 2.75	0.9	50	24	3.8	Decompensated Gain of 6 V/V stable CMOS Amplifier

6 Pin Configuration and Functions

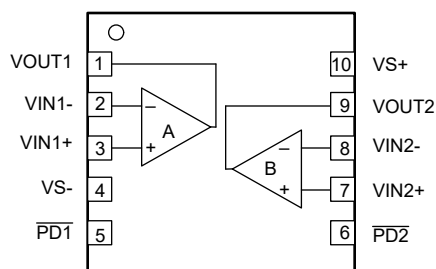


**Figure 6-1. OPA863A DBV Package (Preview),
5-Pin SOT-23
(Top View)**

Table 6-1. Pin Functions

PIN		TYPE ⁽¹⁾	DESCRIPTION
NAME	NO.		
PD	—	I	Power down. Low = disabled, high = enabled
VIN+	3	I	Noninverting input pin
VIN–	4	I	Inverting input pin
VOUT	1	O	Output pin
VS–	2	P	Negative power-supply pin
VS+	5	P	Positive power-supply pin

(1) I = input, O = output, and P = power.



**Figure 6-2. OPA2863A DSN Package,
10-Pin USON with Exposed Power Pad
(Top View)**

Table 6-2. Pin Functions

PIN		TYPE ⁽¹⁾	DESCRIPTION
NAME	NO.		
PD1	5	I	Amplifier 1 power down. Low = disabled, high = enabled
PD2	6	I	Amplifier 2 power down. Low = disabled, high = enabled
VIN1-	2	I	Amplifier 1 inverting input pin
VIN1+	3	I	Amplifier 1 noninverting input pin
VIN2-	8	I	Amplifier 2 inverting input pin
VIN2+	7	I	Amplifier 2 noninverting input pin
VOUT1	1	O	Amplifier 1 output pin
VOUT2	9	O	Amplifier 2 output pin
VS-	4	P	Negative power-supply pin
VS+	10	P	Positive power-supply pin
Power Pad		—	Power pad. Electrically isolated from the device. Recommended connection to a heat spreading plane, typically GND.

(1) I = input, O = output, and P = power.

7 Specifications

7.1 Absolute Maximum Ratings

over operating free-air temperature range (unless otherwise noted)⁽¹⁾

		MIN	MAX	UNIT
V_{S-} to V_{S+}	Supply voltage		13	V
	Supply turn-on/off maximum dV/dt		1	V/ μ s
V_I	Input voltage	$V_{S-} - 0.5$	$V_{S+} + 0.5$	V
V_{ID}	Differential input voltage		± 1	V
I_I	Continuous input current ⁽²⁾		± 10	mA
I_O	Continuous output current ⁽³⁾		± 30	mA
	Continuous power dissipation	See Thermal Information		
T_J	Maximum junction temperature		150	$^{\circ}$ C
T_A	Operating free-air temperature	-40	125	$^{\circ}$ C
T_{stg}	Storage temperature	-65	150	$^{\circ}$ C

- (1) Operation outside the *Absolute Maximum Ratings* may cause permanent device damage. *Absolute Maximum Ratings* do not imply functional operation of the device at these or any other conditions beyond those listed under *Recommended Operating Conditions*. If used outside the *Recommended Operating Conditions* but within the *Absolute Maximum Ratings*, the device may not be fully functional, and this may affect device reliability, functionality, performance, and shorten the device lifetime.
- (2) Continuous input current limit for both the ESD diodes to supply pins and amplifier differential input clamp diode. The differential input clamp diode limits the voltage across it to 1 V with this continuous input current flowing through it.
- (3) Long-term continuous current for electromigration limits.

7.2 ESD Ratings

			VALUE	UNIT
$V_{(ESD)}$	Electrostatic discharge	Human body model (HBM), per ANSI/ESDA/JEDEC JS-001 ⁽¹⁾	± 2000	V
		Charged device model (CDM), per JEDEC specification JESD22 ⁽²⁾	± 1000	

- (1) JEDEC document JEP155 states that 500-V HBM allows safe manufacturing with a standard ESD control process.
- (2) JEDEC document JEP157 states that 250-V CDM allows safe manufacturing with a standard ESD control process.

7.3 Recommended Operating Conditions

over operating free-air temperature range (unless otherwise noted)

		MIN	NOM	MAX	UNIT
$V_{S+} - V_{S-}$	Total supply voltage	2.7	10	12.6	V
T_A	Ambient temperature	-40	25	125	$^{\circ}$ C

7.4 Thermal Information

THERMAL METRIC		OPA2863A	UNIT
		DSN (USON)	
		10 PINS	
$R_{\theta JA}$	Junction-to-ambient thermal resistance	52.4	$^{\circ}$ C/W
$R_{\theta JC(top)}$	Junction-to-case (top) thermal resistance	41.7	$^{\circ}$ C/W
$R_{\theta JB}$	Junction-to-board thermal resistance	25.5	$^{\circ}$ C/W
Ψ_{JT}	Junction-to-top characterization parameter	0.6	$^{\circ}$ C/W
Y_{JB}	Junction-to-board characterization parameter	25.5	$^{\circ}$ C/W
$R_{\theta JC(bot)}$	Junction-to-case (bottom) thermal resistance	8.1	$^{\circ}$ C/W

7.5 Electrical Characteristics: $V_S = \pm 5\text{ V}$

at $G = 1\text{ V/V}$, $R_F = 0\ \Omega$ for $G = 1\text{ V/V}$, otherwise $R_F = 1\text{ k}\Omega$ for other gains, $C_L = 1\text{ pF}$, $R_L = 2\text{ k}\Omega$ referenced to mid-supply, input and output common-mode is at mid-supply, and $T_A \approx 25^\circ\text{C}$ (unless otherwise noted)

PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT
AC PERFORMANCE						
SSBW	Small-signal bandwidth	$V_{OUT} = 20\text{ mV}_{PP}$, $G = 1$		105		MHz
GBWP	Gain-bandwidth product			50		MHz
LSBW	Large-signal bandwidth	$V_{OUT} = 2\text{ V}_{PP}$		14		MHz
	Bandwidth for 0.1-dB flatness	$V_{OUT} = 20\text{ mV}_{PP}$		15		MHz
SR	Slew rate	$V_{OUT} = 2\text{--V}$ step		100		V/ μs
	Rise, fall time	$V_{OUT} = 200\text{--mV}$ step		9		ns
	Settling time to 0.1%	$V_{OUT} = 2\text{--V}$ step		50		ns
	Settling time to 0.01%	$V_{OUT} = 2\text{--V}$ step		70		ns
	Overshoot/undershoot	$V_{OUT} = 2\text{--V}$ step		1		%
	Overdrive recovery time	$G = -1$, 0.5 V overdrive beyond supplies		70		ns
	Overdrive recovery time	$G = 1$, 0.5 V overdrive beyond supplies		90		ns
HD2	Second-order harmonic distortion	$f = 20\text{ kHz}$, $V_{OUT} = 2\text{ V}_{PP}$		-129		dBc
HD3	Third-order harmonic distortion			-138		
HD2	Second-order harmonic distortion	$f = 100\text{ kHz}$, $V_{OUT} = 2\text{ V}_{PP}$		-107		dBc
HD3	Third-order harmonic distortion			-125		
e_N	Input voltage noise			6.3		nV/ $\sqrt{\text{Hz}}$
i_N	Input current noise			0.5		pA/ $\sqrt{\text{Hz}}$
	Closed-loop output impedance	$f = 1\text{ MHz}$		0.2		Ω
	Channel-to-channel crosstalk	$f = 1\text{ MHz}$, $V_{OUT} = 2\text{ V}_{PP}$		-120		dBc
DC PERFORMANCE						
A_{OL}	Open-loop voltage gain	$V_{OUT} = \pm 2.5\text{ V}$	110	128		dB
V_{OS}	Input-referred offset voltage		-95	± 10	95	μV
	Input offset voltage drift	$T_A = -40^\circ\text{C}$ to $+125^\circ\text{C}$	-1.2	± 0.3	1.2	$\mu\text{V}/^\circ\text{C}$
	Input bias current	$T_A \approx 25^\circ\text{C}$		0.3	0.73	μA
		$T_A = -40^\circ\text{C}$ to $+85^\circ\text{C}$			1.2	
		$T_A = -40^\circ\text{C}$ to $+125^\circ\text{C}$			1.6	
	Input bias current drift	$T_A = -40^\circ\text{C}$ to $+125^\circ\text{C}$		± 3		nA/ $^\circ\text{C}$
	Input offset current		-30	± 10	30	nA
INPUT						
	Input common-mode voltage range		$V_{S-}-0.2$		$V_{S+}+0.2$	V
CMRR	Common-mode rejection ratio	$V_{CM} = V_{S-} - 0.2\text{ V}$ to $V_{S+} - 1.6\text{ V}$	95	120		dB
	Input impedance common-mode			650 0.8		M Ω pF
	Input impedance differential mode			200 0.5		k Ω pF
OUTPUT						
V_{OL}	Output voltage, low	$T_A \approx 25^\circ\text{C}$		$V_{S-}+0.14$	$V_{S-}+0.2$	V
		$T_A = -40^\circ\text{C}$ to $+125^\circ\text{C}$		$V_{S-}+0.15$	$V_{S-}+0.22$	
V_{OH}	Output voltage, high	$T_A \approx 25^\circ\text{C}$	$V_{S+}-0.2$	$V_{S+}-0.14$		V
		$T_A = -40^\circ\text{C}$ to $+125^\circ\text{C}$	$V_{S+}-0.2$	$V_{S+}-0.15$		
	Linear output drive (sourcing/sinking)	$V_{OUT} = \pm 2.5\text{ V}$, $\Delta V_{OS} < 1\text{ mV}^{(2)}$	23	30		mA
	Short-circuit current			45		mA
POWER SUPPLY						

7.5 Electrical Characteristics: $V_S = \pm 5\text{ V}$ (continued)

at $G = 1\text{ V/V}$, $R_F = 0\ \Omega$ for $G = 1\text{ V/V}$, otherwise $R_F = 1\text{ k}\Omega$ for other gains, $C_L = 1\text{ pF}$, $R_L = 2\text{ k}\Omega$ referenced to mid-supply, input and output common-mode is at mid-supply, and $T_A \approx 25^\circ\text{C}$ (unless otherwise noted)

PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT
I_Q	Quiescent current per amplifier	$T_A \approx 25^\circ\text{C}$		800	925	μA
		$T_A = -40^\circ\text{C}$ to $+125^\circ\text{C}$			1040	
PSRR	Power-supply rejection ratio	$\Delta V_S = \pm 2\text{ V}^{(1)}$	100	120		dB
POWER DOWN						
	Enable voltage threshold	Specified <i>on</i> above $V_{S+} - 0.5\text{ V}$			4.5	V
	Disable voltage threshold	Specified <i>off</i> below $V_{S+} - 1.5\text{ V}$	3.5			V
	Power-down quiescent current per channel	$V_{PD} \leq V_{S+} - 1.5\text{ V}$		11	28	μA
		$V_{PD} \leq V_{S+} - 1.5\text{ V}$, $T_A = -40^\circ\text{C}$ to $+125^\circ\text{C}$			35	
	Power-down pin bias current			1	2.5	μA
	Turn-on time delay			8		μs
	Turn-off time delay			3.5		μs
AUXILIARY INPUT STAGE						
	Gain-bandwidth product			50		MHz
	Input voltage noise			6.3		$\text{nV}/\sqrt{\text{Hz}}$
	Input current noise			0.5		$\text{pA}/\sqrt{\text{Hz}}$
	Input-referred offset voltage		-95	± 10	95	μV
	Input bias current	$T_A \approx 25^\circ\text{C}$		0.2	0.6	μA
		$T_A = -40^\circ\text{C}$ to $+125^\circ\text{C}$			1.3	
	Common-mode rejection ratio	$V_{CM} = 4.1\text{ V}$ to 5.2 V		120		dB
	Power supply rejection ratio	$\Delta V_S = \pm 0.6\text{ V}$		120		dB

- (1) Change in supply voltage from the default test condition with only one of the positive or negative supplies changing corresponding to +PSRR and -PSRR.
- (2) Change in input offset voltage from no-load condition.

7.6 Electrical Characteristics: $V_S = 3\text{ V}$

at $G = 1$, $R_F = 0\ \Omega$ for $G = 1\text{ V/V}$, otherwise $R_F = 1\text{ k}\Omega$ for other gains, $C_L = 1\text{ pF}$, $R_L = 2\text{ k}\Omega$ connected to 1 V , input and output $V_{CM} = 1\text{ V}$, and $T_A \approx 25^\circ\text{C}$ (unless otherwise noted)

PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT
AC PERFORMANCE						
SSBW	Small-signal bandwidth	$V_{OUT} = 20\text{ mV}_{PP}$, $G = 1$		85		MHz
GBWP	Gain-bandwidth product			50		MHz
LSBW	Large-signal bandwidth	$V_{OUT} = 1\text{ V}_{PP}$		23		MHz
	Bandwidth for 0.1-dB flatness	$V_{OUT} = 20\text{ mV}_{PP}$		10		MHz
SR	Slew rate	$V_{OUT} = 1\text{--V}$ step		53		V/ μs
	Rise, fall time	$V_{OUT} = 200\text{--mV}$ step		10		ns
	Settling time to 0.1%	$V_{OUT} = 1\text{--V}$ step		58		ns
	Settling time to 0.01%			90		
	Overshoot	$V_{OUT} = 1\text{--V}$ step		2		%
	Undershoot			16		
	Overdrive recovery time	$G = -1$, 0.5V overdrive beyond supplies		85		ns
	Overdrive recovery time	$G = 1$, 0.5V overdrive beyond supplies		130		ns
HD2	Second-order harmonic distortion	$f = 20\text{ kHz}$, $V_{OUT} = 1\text{ V}_{PP}$		-123		dBc
HD3	Third-order harmonic distortion			-132		
HD2	Second-order harmonic distortion	$f = 100\text{ kHz}$, $V_{OUT} = 1\text{ V}_{PP}$		-109		dBc
HD3	Third-order harmonic distortion			-129		
e_N	Input voltage noise			6.3		nV/ $\sqrt{\text{Hz}}$
i_N	Input current noise			0.5		pA/ $\sqrt{\text{Hz}}$
	Closed-loop output impedance	$f = 1\text{ MHz}$		0.2		Ω
	Channel-to-channel crosstalk	$f = 1\text{ MHz}$, $V_{OUT} = 1\text{ V}_{PP}$		-120		dBc
DC PERFORMANCE						
A_{OL}	Open-loop voltage gain	$V_{OUT} = 1\text{ V}$ to 2 V	104	123		dB
V_{OS}	Input-referred offset voltage		-95	± 10	95	μV
	Input offset voltage drift	$T_A = -40^\circ\text{C}$ to $+125^\circ\text{C}$	-1.2	± 0.3	1.2	$\mu\text{V}/^\circ\text{C}$
	Input bias current	$T_A \approx 25^\circ\text{C}$		0.3	0.73	μA
		$T_A = -40^\circ\text{C}$ to $+85^\circ\text{C}$			1.2	
		$T_A = -40^\circ\text{C}$ to $+125^\circ\text{C}$			1.56	
	Input bias current drift	$T_A = -40^\circ\text{C}$ to $+125^\circ\text{C}$		± 3		nA/ $^\circ\text{C}$
	Input offset current		-30	± 10	30	nA
INPUT						
	Input common-mode voltage range		$V_{S-}-0.2$	$V_{S+}+0.2$		V
CMRR	Common-mode rejection ratio	$V_{CM} = V_{S-} - 0.2\text{ V}$ to $V_{S+} - 1.6\text{ V}$	92	115		dB
	Input impedance common-mode			360 0.9		M Ω pF
	Input impedance differential mode			200 0.5		k Ω pF
OUTPUT						
V_{OL}	Output voltage, low	$T_A \approx 25^\circ\text{C}$		$V_{S-}+0.13$	$V_{S-}+0.15$	V
		$T_A = -40^\circ\text{C}$ to $+125^\circ\text{C}$		$V_{S-}+0.13$	$V_{S-}+0.16$	
V_{OH}	Output voltage, high	$T_A \approx 25^\circ\text{C}$	$V_{S+}-0.15$	$V_{S+}-0.13$		V
		$T_A = -40^\circ\text{C}$ to $+125^\circ\text{C}$	$V_{S+}-0.15$	$V_{S+}-0.13$		
	Linear output drive (sourcing/sinking)	$V_{OUT} = \pm 0.7\text{ V}$, $\Delta V_{OS} < 1\text{ mV}^{(2)}$	23	33		mA
	Short-circuit current			45		mA

7.6 Electrical Characteristics: $V_S = 3\text{ V}$ (continued)

at $G = 1$, $R_F = 0\ \Omega$ for $G = 1\text{ V/V}$, otherwise $R_F = 1\text{ k}\Omega$ for other gains, $C_L = 1\text{ pF}$, $R_L = 2\text{ k}\Omega$ connected to 1 V , input and output $V_{CM} = 1\text{ V}$, and $T_A \approx 25^\circ\text{C}$ (unless otherwise noted)

PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT
POWER SUPPLY						
I_Q	Quiescent current per amplifier	$T_A \approx 25^\circ\text{C}$		770	890	μA
		$T_A = -40^\circ\text{C}$ to $+125^\circ\text{C}$			995	
PSRR	Power-supply rejection ratio	$\Delta V_S = \pm 1\text{ V}^{(1)}$	100	120		dB
POWER DOWN						
	Enable voltage threshold	Specified <i>on</i> above $V_{S+} - 0.5\text{ V}$			2.5	V
	Disable voltage threshold	Specified <i>off</i> below $V_{S+} - 1.5\text{ V}$	1.5			V
	Power-down quiescent current per channel	$V_{PD} \leq V_{S+} - 1.5\text{ V}$		8.5	20	μA
		$V_{PD} \leq V_{S+} - 1.5\text{ V}$, $T_A = -40^\circ\text{C}$ to $+125^\circ\text{C}$			30	
	Power-down pin bias current			1	2.5	μA
	Turn-on time delay			8		μs
	Turn-off time delay			3.5		μs
AUXILIARY INPUT STAGE						
	Gain-bandwidth product			50		MHz
	Input voltage noise			6.3		nV/ $\sqrt{\text{Hz}}$
	Input current noise			0.5		pA/ $\sqrt{\text{Hz}}$
	Input-referred offset voltage		-95	± 10	95	μV
	Input bias current	$T_A \approx 25^\circ\text{C}$		0.2	0.6	μA
		$T_A = -40^\circ\text{C}$ to $+125^\circ\text{C}$			1.2	
	Common-mode rejection ratio	$V_{CM} = 2.1\text{ V}$ to 3.2 V		115		dB
	Power supply rejection ratio	$\Delta V_S = \pm 0.6\text{ V}$		115		dB

- (1) Change in supply voltage from the default test condition with only one of the positive or negative supplies changing corresponding to +PSRR and -PSRR.
- (2) Change in input offset voltage from no-load condition.

7.7 Typical Characteristics: $V_S = \pm 5\text{ V}$

at $V_{S+} = 5\text{ V}$, $V_{S-} = -5\text{ V}$, $R_F = 0\ \Omega$ for Gain = 1 V/V, otherwise $R_F = 1\text{ k}\Omega$ for other gains, $C_L = 1\text{ pF}$, $R_L = 2\text{ k}\Omega$ referenced to mid-supply, $G = 1\text{ V/V}$, input and output referenced to mid-supply, and $T_A \approx 25^\circ\text{C}$ (unless otherwise noted)

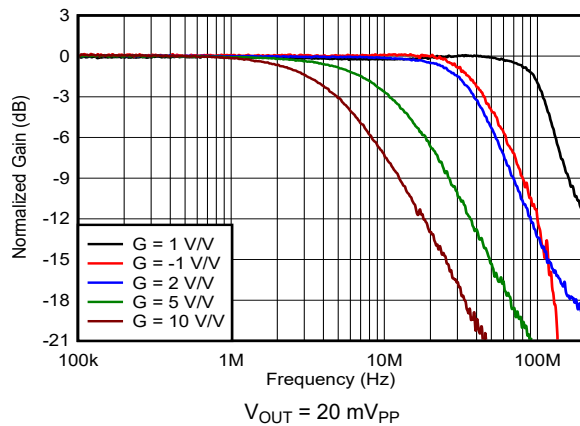


Figure 7-1. Small-Signal Frequency Response vs Gain

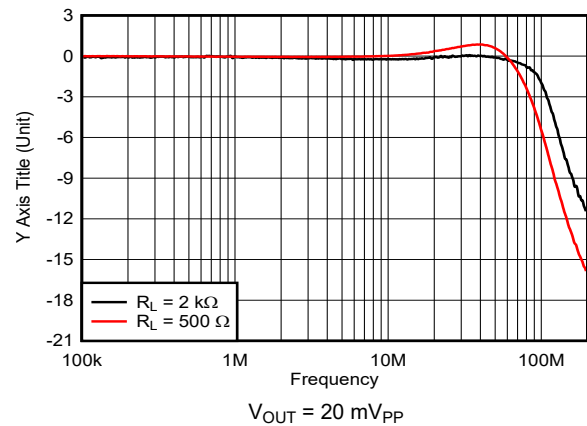


Figure 7-2. Small-Signal Frequency Response vs Output Load

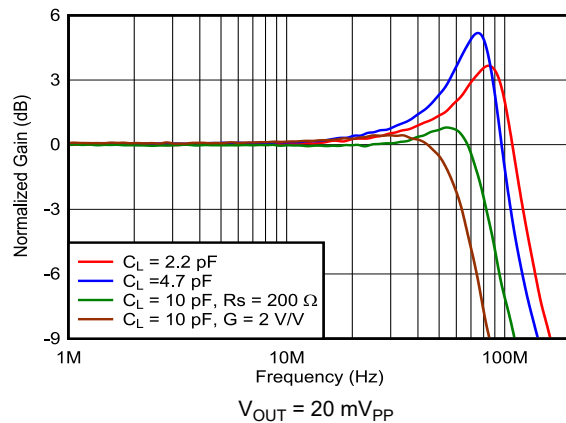


Figure 7-3. Frequency Response vs Load Capacitance

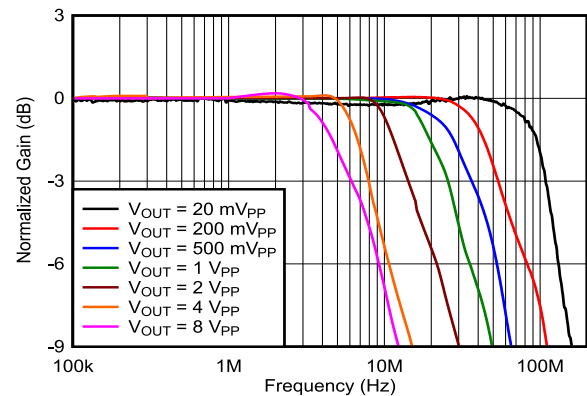


Figure 7-4. Frequency Response vs Output Voltage

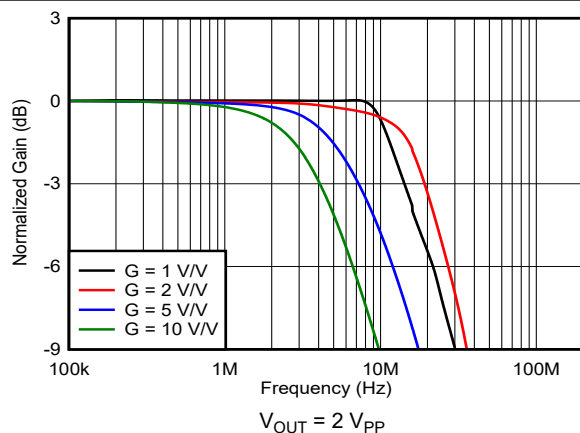


Figure 7-5. Large-Signal Frequency Response vs Gain

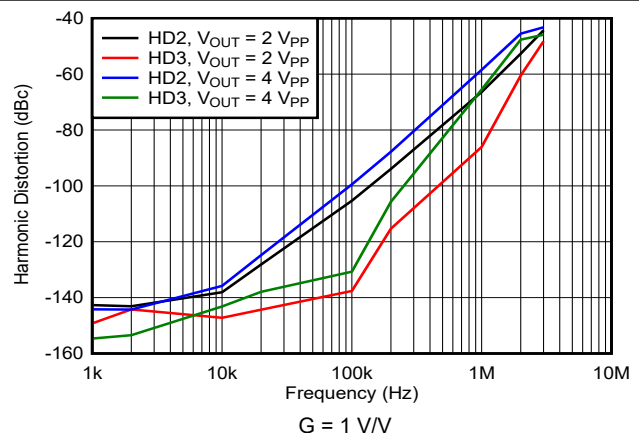


Figure 7-6. Harmonic Distortion vs Frequency

7.7 Typical Characteristics: $V_S = \pm 5\text{ V}$ (continued)

at $V_{S+} = 5\text{ V}$, $V_{S-} = -5\text{ V}$, $R_F = 0\ \Omega$ for Gain = 1 V/V, otherwise $R_F = 1\text{ k}\Omega$ for other gains, $C_L = 1\text{ pF}$, $R_L = 2\text{ k}\Omega$ referenced to mid-supply, $G = 1\text{ V/V}$, input and output referenced to mid-supply, and $T_A \approx 25^\circ\text{C}$ (unless otherwise noted)

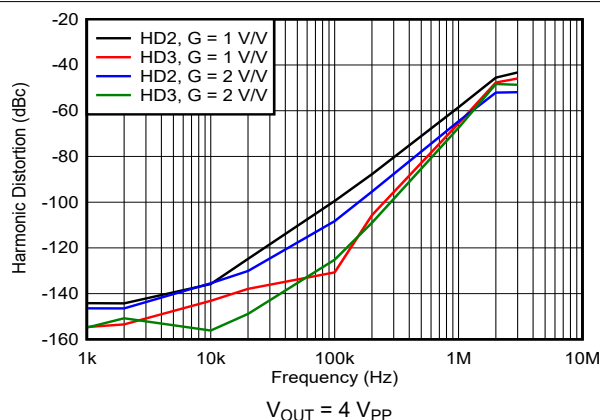


Figure 7-7. Harmonic Distortion vs Gain

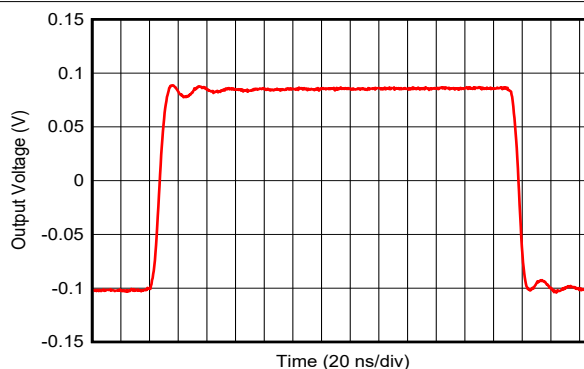


Figure 7-8. Small-Signal Transient Response

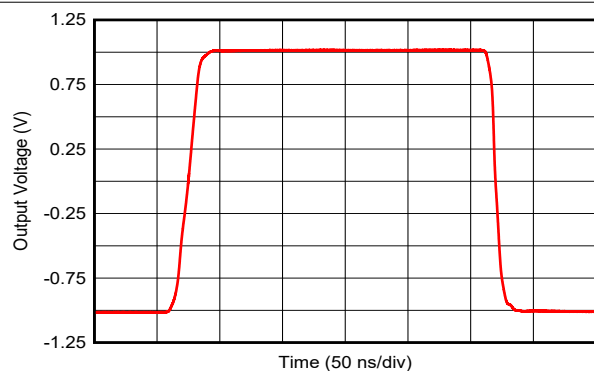


Figure 7-9. Large-Signal Transient Response

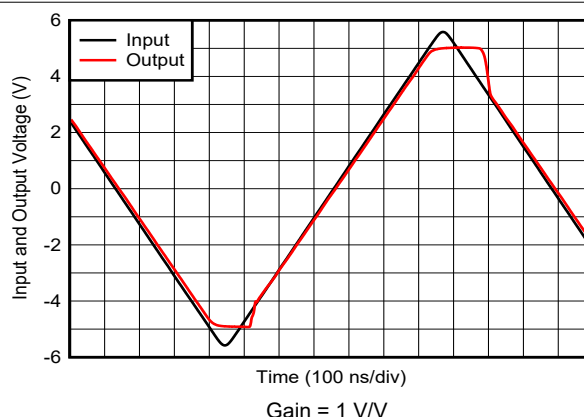


Figure 7-10. Input Overdrive Recovery

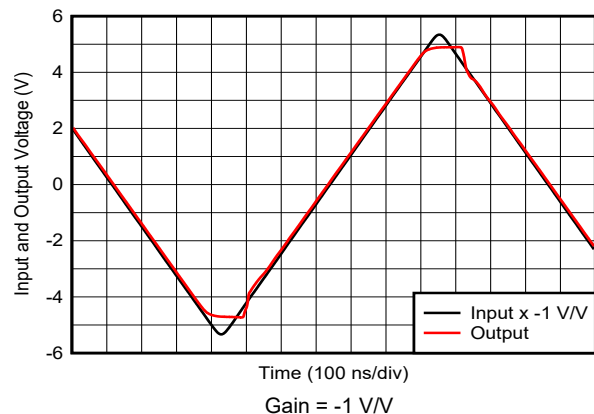


Figure 7-11. Output Overdrive Recovery

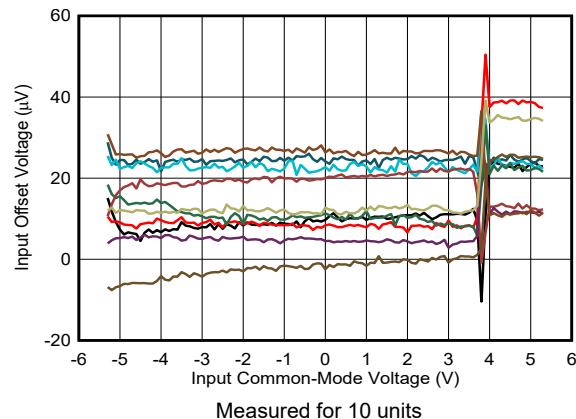


Figure 7-12. Input Offset Voltage vs Input Common-Mode Voltage

7.7 Typical Characteristics: $V_S = \pm 5\text{ V}$ (continued)

at $V_{S+} = 5\text{ V}$, $V_{S-} = -5\text{ V}$, $R_F = 0\ \Omega$ for Gain = 1 V/V, otherwise $R_F = 1\text{ k}\Omega$ for other gains, $C_L = 1\text{ pF}$, $R_L = 2\text{ k}\Omega$ referenced to mid-supply, $G = 1\text{ V/V}$, input and output referenced to mid-supply, and $T_A \approx 25^\circ\text{C}$ (unless otherwise noted)

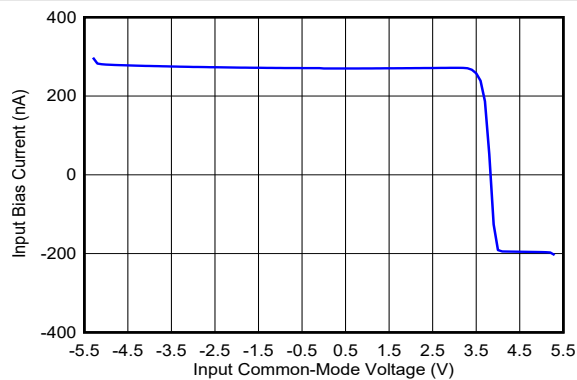


Figure 7-13. Input Bias Current vs Input Common-Mode Voltage

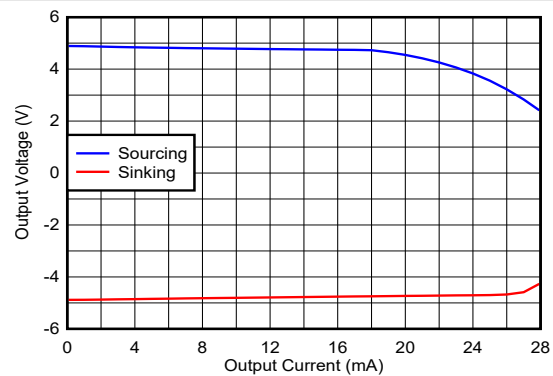
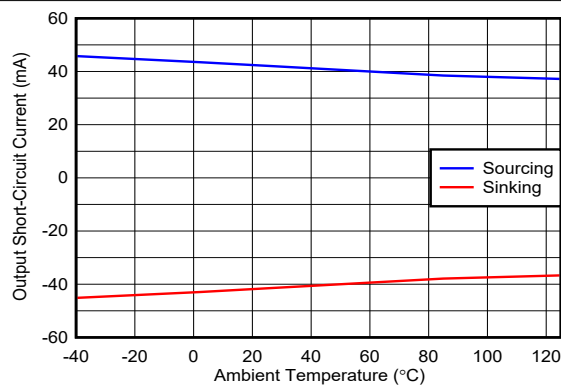


Figure 7-14. Output Voltage vs Load Current



Output saturated and then short-circuited to opposite supply

Figure 7-15. Output Short-Circuit Current vs Ambient Temperature

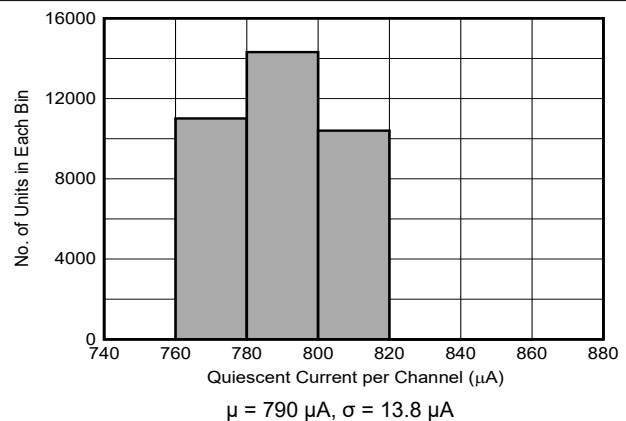


Figure 7-16. Quiescent Current Distribution

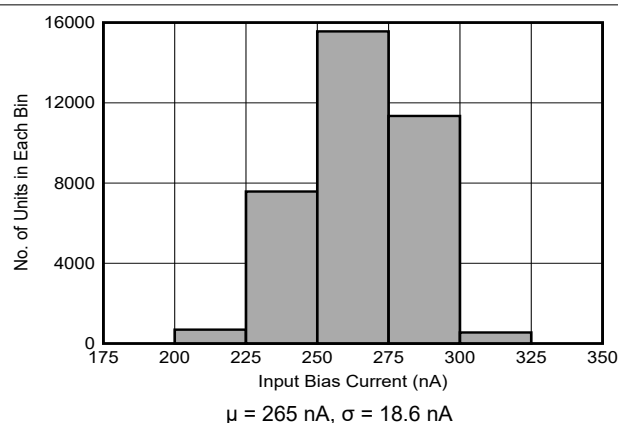


Figure 7-17. Input Bias Current Distribution

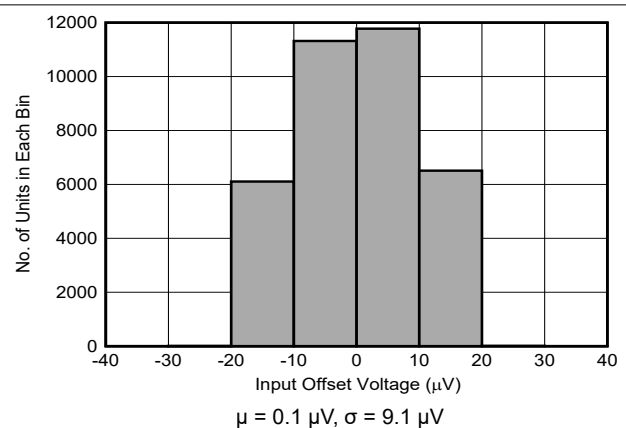


Figure 7-18. Input Offset Voltage Distribution

7.7 Typical Characteristics: $V_S = \pm 5\text{ V}$ (continued)

at $V_{S+} = 5\text{ V}$, $V_{S-} = -5\text{ V}$, $R_F = 0\ \Omega$ for Gain = 1 V/V, otherwise $R_F = 1\text{ k}\Omega$ for other gains, $C_L = 1\text{ pF}$, $R_L = 2\text{ k}\Omega$ referenced to mid-supply, $G = 1\text{ V/V}$, input and output referenced to mid-supply, and $T_A \cong 25^\circ\text{C}$ (unless otherwise noted)

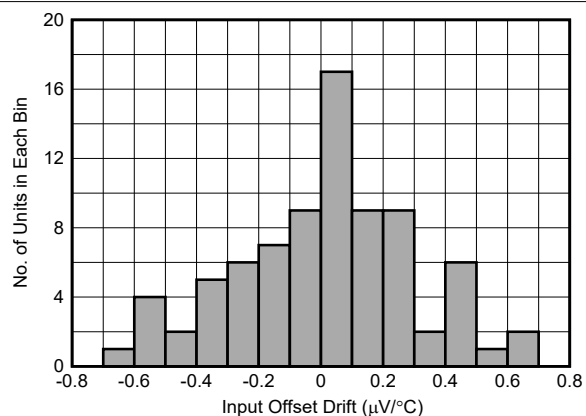


Figure 7-19. Input Offset Voltage Drift Distribution

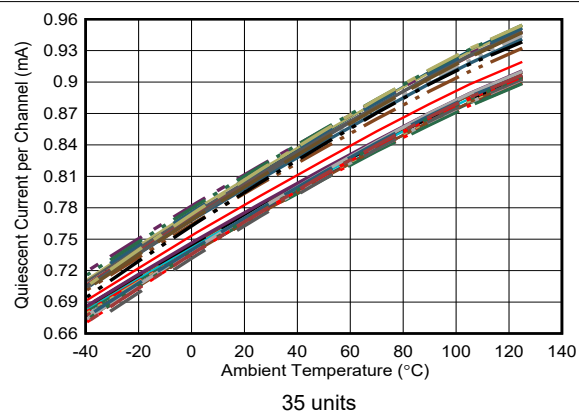


Figure 7-20. Quiescent Current vs Ambient Temperature

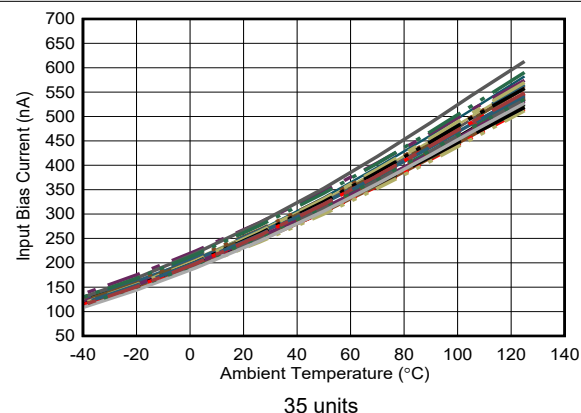


Figure 7-21. Input Bias Current vs Ambient Temperature

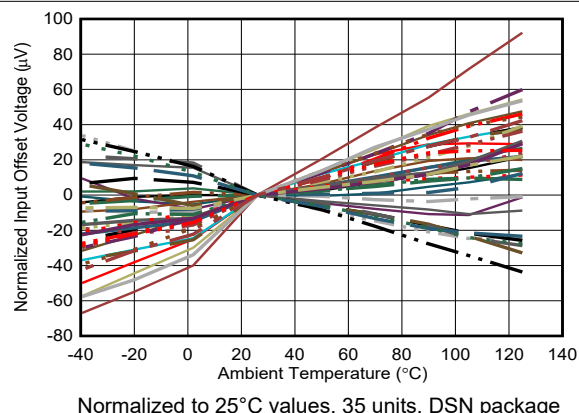


Figure 7-22. Input Offset Voltage vs Ambient Temperature

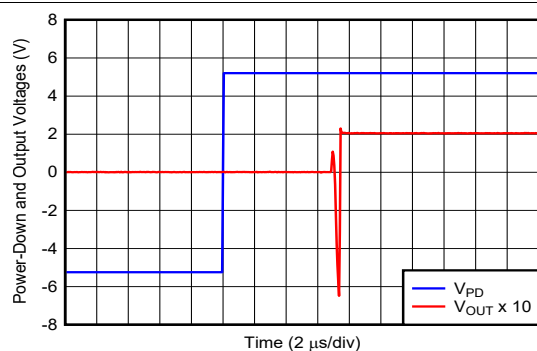


Figure 7-23. Turn-On Time to DC Input

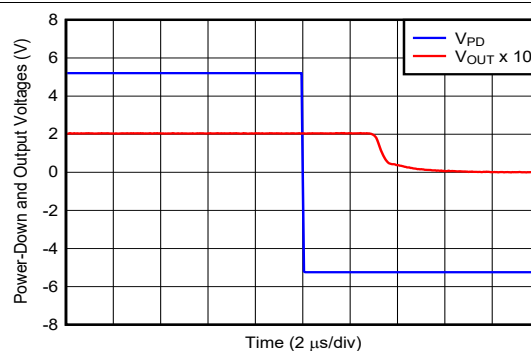


Figure 7-24. Turn-Off Time to DC Input

7.7 Typical Characteristics: $V_S = \pm 5\text{ V}$ (continued)

at $V_{S+} = 5\text{ V}$, $V_{S-} = -5\text{ V}$, $R_F = 0\ \Omega$ for Gain = 1 V/V, otherwise $R_F = 1\text{ k}\Omega$ for other gains, $C_L = 1\text{ pF}$, $R_L = 2\text{ k}\Omega$ referenced to mid-supply, $G = 1\text{ V/V}$, input and output referenced to mid-supply, and $T_A \approx 25^\circ\text{C}$ (unless otherwise noted)

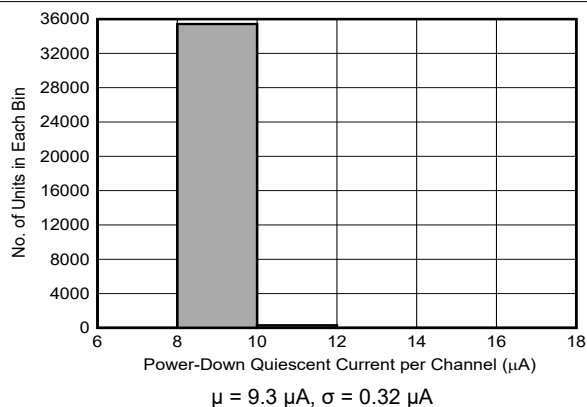


Figure 7-25. Power-Down Quiescent Current Distribution

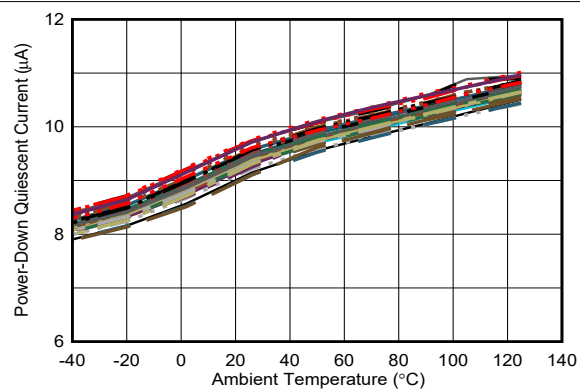


Figure 7-26. Power-Down I_Q vs Ambient Temperature

7.8 Typical Characteristics: $V_S = 3\text{ V}$

at $V_{S+} = 3\text{ V}$, $V_{S-} = 0\text{ V}$, $R_F = 0\ \Omega$ for Gain = 1 V/V, otherwise $R_F = 1\text{ k}\Omega$ for other gains, $C_L = 1\text{ pF}$, $R_L = 2\text{ k}\Omega$ connected to 1 V, $G = 1\text{ V/V}$, input and output $V_{CM} = 1\text{ V}$, and $T_A \approx 25^\circ\text{C}$ (unless otherwise noted)

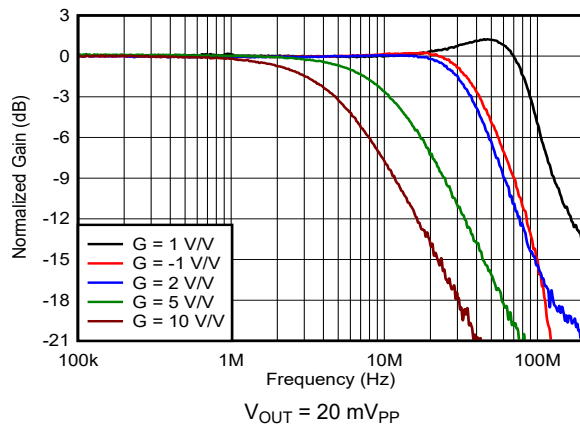


Figure 7-27. Small-Signal Frequency Response vs Gain

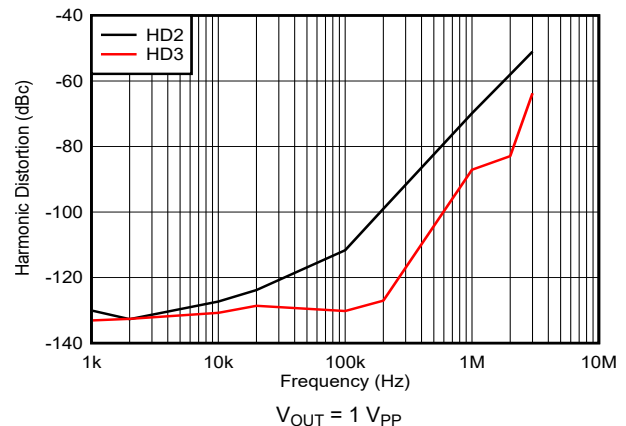


Figure 7-28. Harmonic Distortion vs Frequency

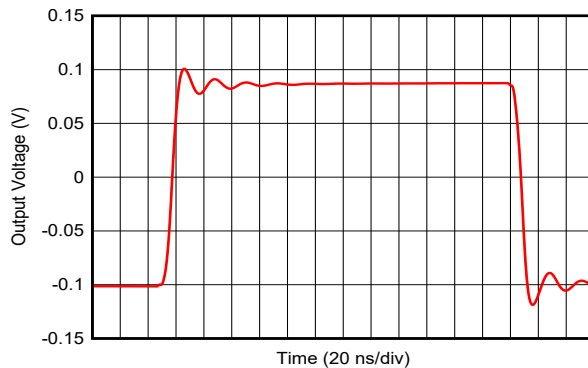


Figure 7-29. Small-Signal Transient Response

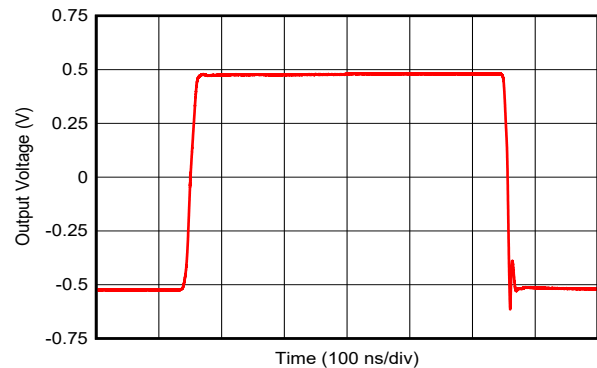


Figure 7-30. Large-Signal Transient Response

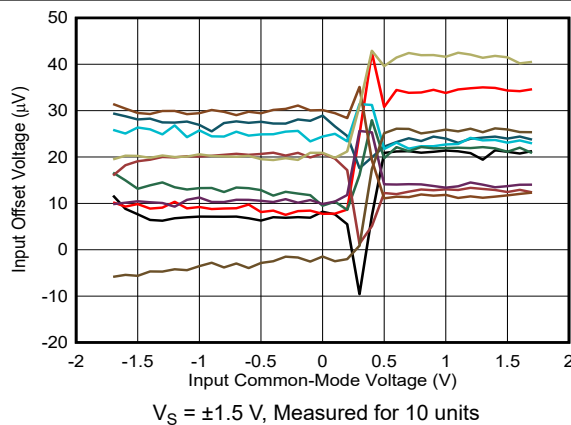


Figure 7-31. Input Offset Voltage vs Input Common-Mode Voltage

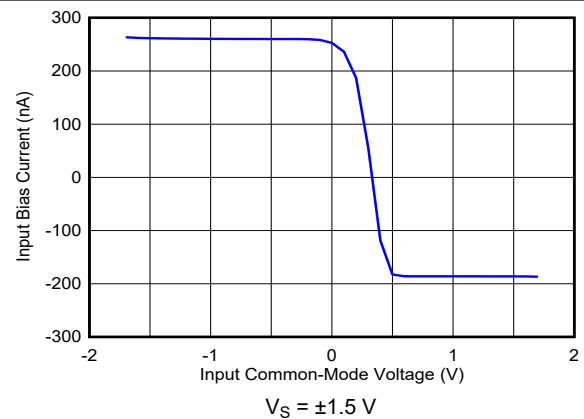


Figure 7-32. Input Bias Current vs Input Common-Mode Voltage

7.8 Typical Characteristics: $V_S = 3\text{ V}$ (continued)

at $V_{S+} = 3\text{ V}$, $V_{S-} = 0\text{ V}$, $R_F = 0\ \Omega$ for Gain = 1 V/V, otherwise $R_F = 1\text{ k}\Omega$ for other gains, $C_L = 1\text{ pF}$, $R_L = 2\text{ k}\Omega$ connected to 1 V, $G = 1\text{ V/V}$, input and output $V_{CM} = 1\text{ V}$, and $T_A \approx 25^\circ\text{C}$ (unless otherwise noted)

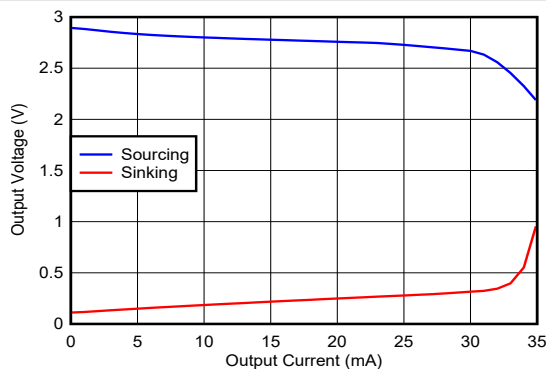
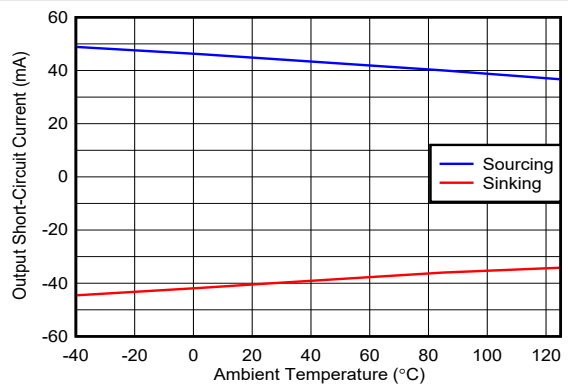


Figure 7-33. Output Voltage vs Load Current



Output saturated and then short-circuited to other supply

Figure 7-34. Output Short-Circuit Current vs Ambient Temperature

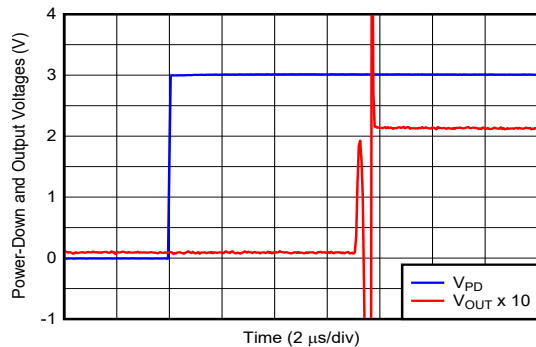


Figure 7-35. Turn-On Time to DC Input

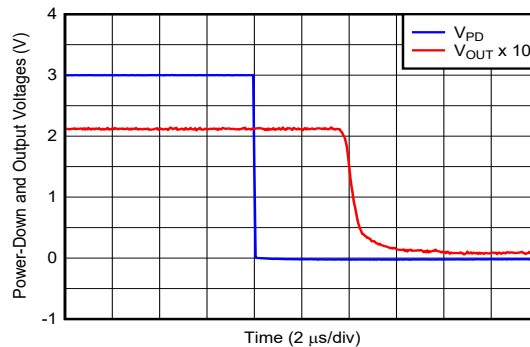


Figure 7-36. Turn-Off Time to DC Input

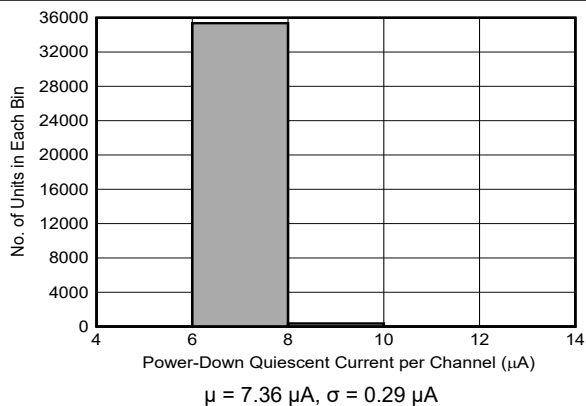


Figure 7-37. Power-Down Quiescent Current Distribution

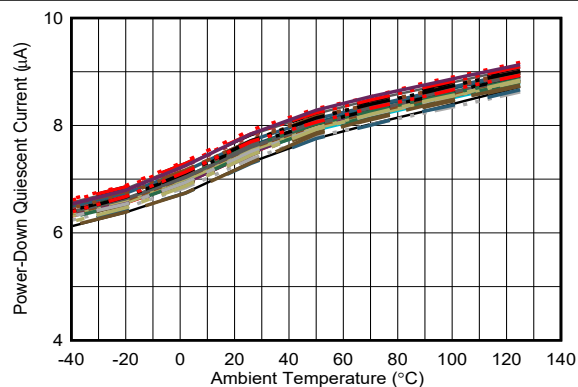


Figure 7-38. Power-Down I_Q vs. Ambient Temperature

7.9 Typical Characteristics: $V_S = 3\text{ V to }10\text{ V}$

at $V_{OUT} = 2\text{ V}_{PP}$, $R_F = 0\ \Omega$ for Gain = 1 V/V, otherwise $R_F = 1\text{ k}\Omega$ for other gains, $C_L = 1\text{ pF}$, $R_L = 2\text{ k}\Omega$ referenced to mid-supply, $G = 1\text{ V/V}$, input and output referenced to mid-supply, and $T_A \approx 25^\circ\text{C}$ (unless otherwise noted)

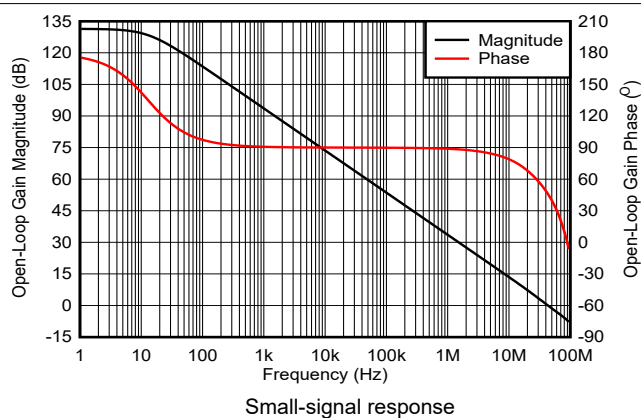


Figure 7-39. Open-Loop Gain and Phase vs Frequency

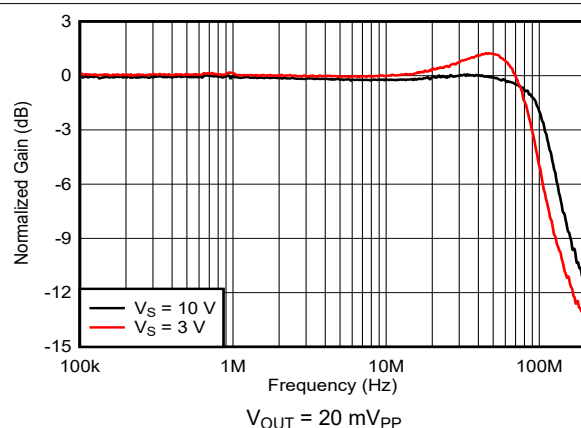


Figure 7-40. Frequency Response vs Supply Voltage

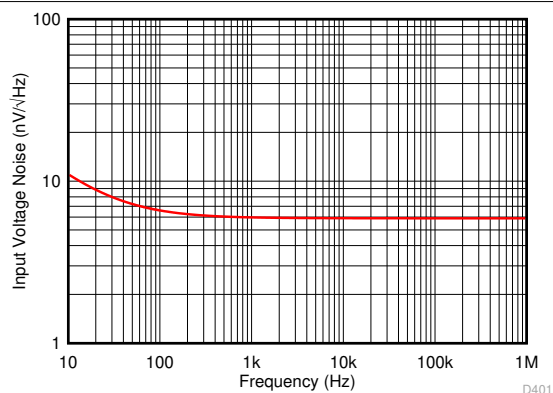


Figure 7-41. Input Voltage Noise Density vs Frequency

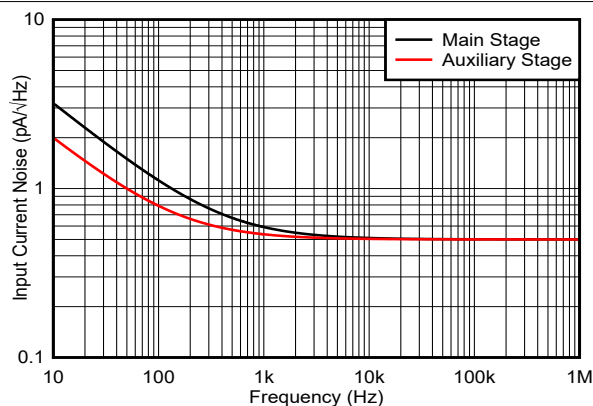


Figure 7-42. Input Current Noise Density vs Frequency

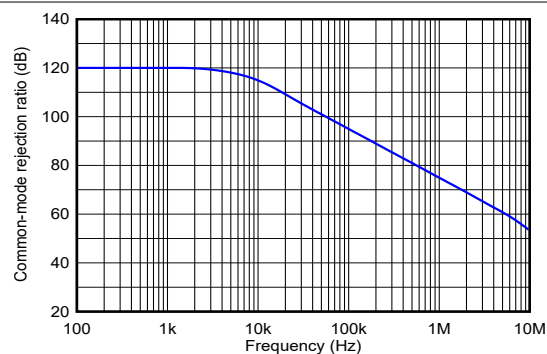


Figure 7-43. Common-Mode Rejection Ratio vs Frequency

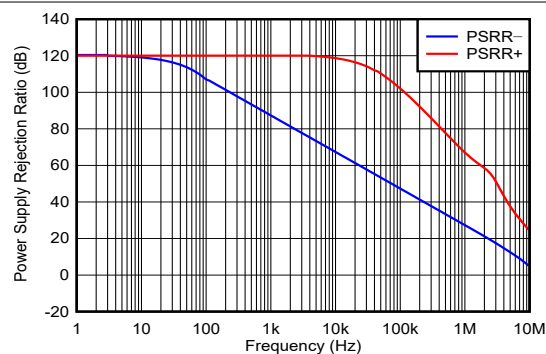


Figure 7-44. Power Supply Rejection Ratio vs Frequency

7.9 Typical Characteristics: $V_S = 3\text{ V to }10\text{ V}$ (continued)

at $V_{OUT} = 2\text{ V}_{PP}$, $R_F = 0\ \Omega$ for Gain = 1 V/V, otherwise $R_F = 1\text{ k}\Omega$ for other gains, $C_L = 1\text{ pF}$, $R_L = 2\text{ k}\Omega$ referenced to mid-supply, $G = 1\text{ V/V}$, input and output referenced to mid-supply, and $T_A \cong 25^\circ\text{C}$ (unless otherwise noted)

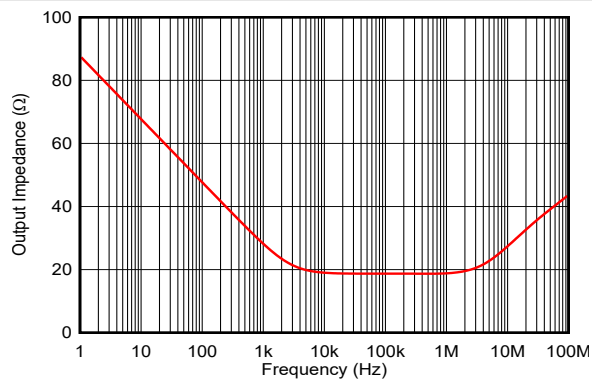


Figure 7-45. Open-Loop Output Impedance vs Frequency

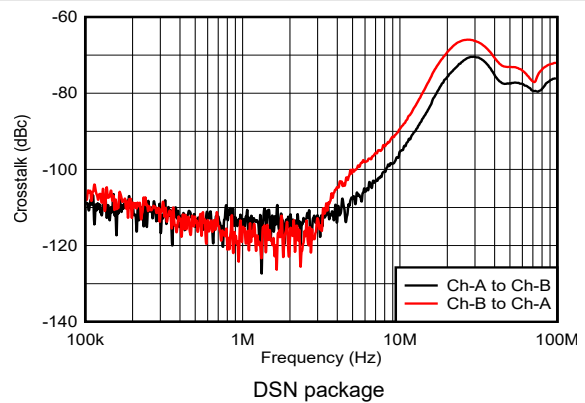


Figure 7-46. Crosstalk vs Frequency

8.3 Feature Description

8.3.1 Input Stage

The OPAx863A devices include a rail-to-rail input stage. The main stage differential pair using PNP bipolar transistors operates for common-mode input voltages from $V_{S-} - 0.2\text{ V}$ till $V_{S+} - 1.6\text{ V}$. The amplifier inputs transition into the auxiliary stage using NPN transistors for common-mode input voltages from $V_{S+} - 1.6\text{ V}$ till $V_{S+} + 0.2\text{ V}$. The PNP and NPN input stages offer a gain-bandwidth product of 50 MHz and a voltage noise density of 6.3 nV/ $\sqrt{\text{Hz}}$. The offset voltage for the two input stages is matched to lie within the device specifications. The auxiliary NPN input stage does not use the slew boost circuit during large-signal transient response. The input bias current for the PNP and NPN input stages is opposite in polarity, which adds an additional offset based on the values of the gain-setting and feedback resistors. A common-mode input voltage transition between these input stages will cause a crossover distortion which needs to be considered in high-frequency applications requiring superior linearity. Limit the common-mode input voltage to $V_{S+} - 1.6\text{ V}$ (maximum) for main-stage operation across process and ambient temperature.

Since the OPAx863A devices are bipolar amplifiers, the two inputs are protected with anti-parallel back-to-back diodes between them, which limits the maximum input differential voltage to 1 V. The amplifier is slew limited, and the two inputs are pulled apart up to 1 V when the anti-parallel diodes begin to conduct in very fast input or output transient conditions. Care must be taken to use gain-setting and feedback resistors large enough to limit the current through these diodes in such conditions.

8.3.2 Output Stage

The OPAx863A devices feature a rail-to-rail output stage with possible signal swing from $V_{S-} + 0.2\text{ V}$ to $V_{S+} - 0.2\text{ V}$. Violating the output headroom to either of the supplies will cause output signal clipping and introduce distortion.

The OPAx863A devices integrate an output short-circuit protection circuit, which makes the device rugged for use in real-world applications.

8.3.2.1 Overload Power Limit

During overload or fault conditions, bipolar rail-to-rail output (RRO) amplifiers consume excessive quiescent current (five to seven times) with saturated outputs. With saturated outputs, the output signal is clipped with much higher base current from output pre-driver stage causing increase in device quiescent current. During this condition, the negative feedback control is disabled and an input differential voltage appears thereby resulting in an input overdrive. During input overdrive, the slew boost circuit engages to increase tail current which further increases device quiescent current. This overall increase in quiescent current can cause excessive battery discharge in portable products shortening operating lifetime or disturb the thermal equilibrium causing irreversible damage due to increased system power dissipation in a multi-channel design.

The OPAx863A includes an intelligent overload detection circuit. This circuit monitors for output saturation and limits the base drive from output pre-driver circuit and disables the slew boost circuit in this condition. As [Table 8-1](#) provides, this feature limits the increase in device quiescent current to much smaller values.

Table 8-1. Quiescent Current with Saturated Outputs

Device	Input Differential Voltage	Quiescent Current during overload	Increase in I_Q from steady-state condition
OPAx863A with overload power limit	500 mV	1.4 mA	1.8x
Competitor amplifier without overload power limit	500 mV	4.05 mA	7.1x

8.3.3 ESD Protection

As [Figure 8-1](#) shows, all device pins are protected with internal ESD protection diodes to the power supplies. These diodes provide moderate protection to input overdrive voltages above the supplies. The protection diodes can typically support 10-mA continuous input and output currents. Use series current limiting resistors if input voltages exceeding the supply voltages occur at the amplifier inputs, which ensures the current through the ESD diodes remains within their rated value. Since OPAx863A is a bipolar amplifier, the two inputs are protected with anti-parallel back-to-back diodes between them which limits the maximum input differential voltage to approximately 1 V. Care must be taken to use gain-setting and feedback resistors large enough to limit the current through these diodes in fast slewing conditions.

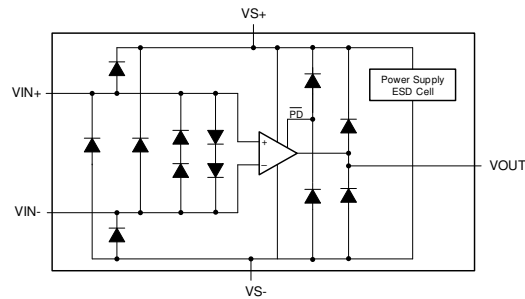


Figure 8-1. Internal ESD Protection

8.4 Device Functional Modes

8.4.1 Power-Down Mode

The OPAx863A includes a power-down mode for low-power standby operation with a quiescent current of 8.5 μ A (typical) and high output impedance. Many low-power systems are active for only a small time interval when the parameters of interest are measured and remain in low-power standby mode for a majority of the time for an overall small average power consumption. The OPAx863A enables such a low-power operation with quick turn-on within less than 8 μ s. Refer to the *Electrical Characteristics* tables for power-down pin control thresholds.

The OPAx863A is enabled with the $\overline{\text{PD}}$ pin driven to $V_{S+} - 0.5$ V or higher. The device powers down if the $\overline{\text{PD}}$ pin is driven to $V_{S+} - 1.5$ V or lower with a driver device capable of sinking approximately 1 μ A (typical) current from the $\overline{\text{PD}}$ pin. If level translation is needed to realize the $\overline{\text{PD}}$ pin thresholds for enable or power-down modes of operation, an external pull-up resistor from $\overline{\text{PD}}$ pin to V_{S+} driven with an open-collector output should be used.

9 Application and Implementation

Note

Information in the following applications sections is not part of the TI component specification, and TI does not warrant its accuracy or completeness. TI's customers are responsible for determining suitability of components for their purposes, as well as validating and testing their design implementation to confirm system functionality.

9.1 Application Information

The OPAx863A devices are classic voltage-feedback amplifiers with each channel having two high-impedance inputs and a low-impedance output. The combination of specifications with a GBW of 50 MHz, 6.3 nV/ $\sqrt{\text{Hz}}$ noise, RRIO capability and high-precision performance consuming only 800 μA quiescent current make it an ideal choice for use in precision data acquisition, reference buffering with fast settling, high gain and filter circuits. The overload power limit makes OPAx863A truly low-power in high-gain multi-channel systems limiting any increase in quiescent current during output overload conditions.

9.2 Typical Applications

9.2.1 Low-Power SAR ADC Driver and Reference Buffer

Figure 9-1 shows the use of the OPAx863A devices as a SAR ADC input driver driving the ADS7057. Sensors, which are used for interface with the physical environment, exhibit high output impedance and cannot drive SAR ADC inputs directly. A wide-GBW amplifier like the OPAx863A devices are needed to charge the switching capacitors at the SAR ADC input and to settle fast to the required accuracy within the given acquisition time. The OPAx863A's wide-GBW, high precision performance enables fast settling, high accuracy sensor measurements, and reference buffering for precision ADCs.

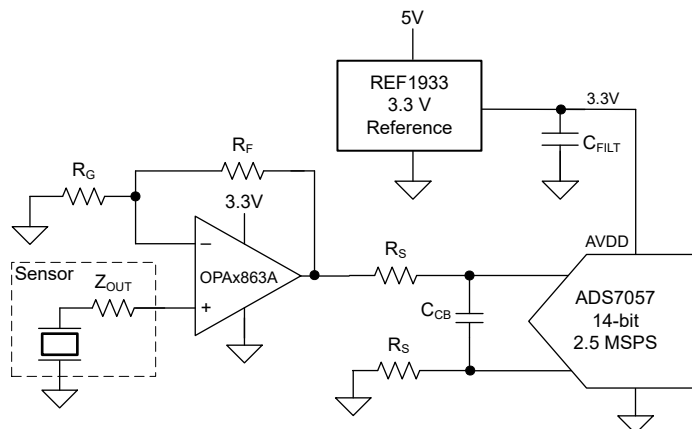


Figure 9-1. OPAx863A as Precision SAR ADC Driver

9.2.2 Active Filters

Active filter circuits are used to amplify signals in the passband, attenuate signals in the stopband and also limit the integrated noise at the amplifier's output. The OPAX863A with its wide bandwidth and high-precision performance is suitable for designing multi-feedback (MFB) low-pass filter circuits.

9.2.2.1 Design Requirements

This section discusses the design of a MFB low-pass active filter with a cut-off frequency at 2 MHz and the impact of amplifier's gain-bandwidth (GBW) on filter performance.

9.2.2.2 Detailed Design Procedure

Figure 9-2 shows the use of OPAX863A in a second-order multi-feedback (MFB) low-pass filter with a cut-off frequency of 2 MHz. The passive component values are first selected for a cut-off frequency at 1 rad/sec and later scaled for 2 MHz. The frequency response of the circuit in Figure 9-2 is compared for various amplifiers with different gain-bandwidth products and shown in Figure 9-3:

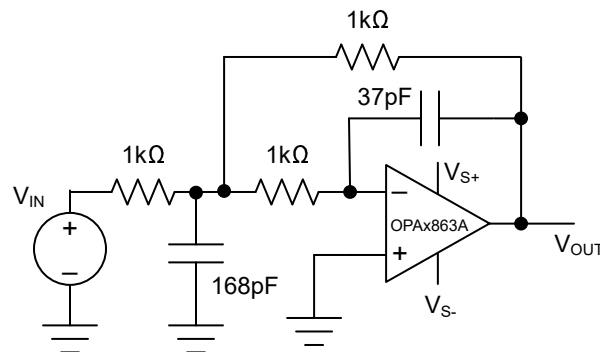


Figure 9-2. MFB Low-Pass Filter Circuit Using OPAX863A

Table 9-1. Impact of amplifier GBW on Cut-Off Frequency

Device	GBW (MHz)	Cut-off frequency (MHz)
TLV9051	5	1.59
LMV641	10	1.78
OPA2834	20	1.87
OPAX863A	50	1.95
OPA836	110	1.98

Table 9-1 provides the following benefits of using OPAX863A in an MFB low-pass filter circuit:

- High precision measurements with low offset voltage across operating temperature range for low-frequency signals in passband
- High linearity due to the larger GBW and loop gain for low-frequency signals in passband
- Higher accuracy of cut-off frequency and its smaller variation over process and temperature
- Small integrated output noise due to low-pass filtering

As Figure 9-3 shows, the amplifier's gain-bandwidth, like the OPAX863A, should be at least 20x greater than the filter cut-off frequency for a high-precision and linearity low-pass filter design.

9.2.2.3 Application Curves

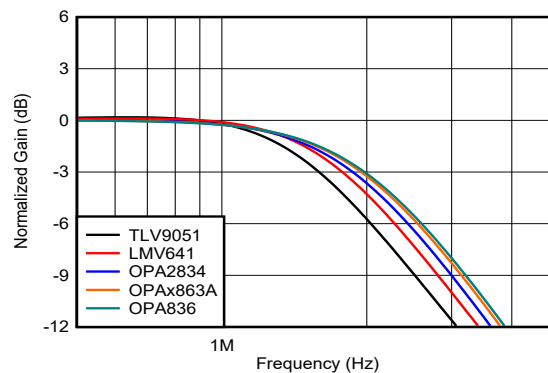


Figure 9-3. MFB Low-Pass Filter Frequency Response vs GBW

10 Power Supply Recommendations

The OPAx863A devices are intended to operate on supplies ranging from 2.7 V to 12.6 V. The OPAx863A devices may operate on single-sided supplies, split and balanced bipolar supplies, or unbalanced bipolar supplies. Operating from a single supply can have numerous advantages. The DC errors, due to the $-PSRR$ term, can be minimized with the negative supply at ground. Typically, AC performance improves slightly at 10-V operation with minimal increase in supply current. Minimize the distance (< 0.1 in) from the power supply pins to high-frequency, 0.01- μ F decoupling capacitors. A larger capacitor (2.2 μ F typical) is used along with a high-frequency, 0.01- μ F supply-decoupling capacitor at the device supply pins. Only the positive supply has these capacitors for single-supply operation. Use these capacitors from each supply to ground when a split-supply is used. If necessary, place the larger capacitors further from the device and share these capacitors among several devices in the same area of the printed circuit board (PCB). An optional supply decoupling capacitor across the two power supplies (for split-supply operation) reduces second harmonic distortion.

11 Layout

11.1 Layout Guidelines

Achieving optimum performance with a high-frequency amplifier (like the OPAx863A devices) require careful attention to board layout parasitics and external component types. The [High Speed Amplifiers Generic DSN Evaluation Module user's guide](#) can be used as a reference when designing the circuit board. Recommendations that optimize performance includes the following:

1. **Minimize parasitic capacitance** to any AC ground for all of the signal I/O pins. Parasitic capacitance on the output and inverting input pins can cause instability on the noninverting input and can react with the source impedance to cause unintentional band-limiting. Open a window around the signal I/O pins in all of the ground and power planes around those pins to reduce unwanted capacitance. Otherwise, ground and power planes must be unbroken elsewhere on the board.
2. **Minimize the distance** (< 0.1 in) from the power-supply pins to high-frequency 0.01- μ F decoupling capacitors. Avoid narrow power and ground traces to minimize inductance between the pins and the decoupling capacitors. The power-supply connections must always be decoupled with these capacitors. Larger (2.2- μ F to 6.8- μ F) decoupling capacitors, effective at lower frequency, must also be used on the supply pins. These can be placed somewhat farther from the device and shared among several devices in the same area of the PC board.
3. **Careful selection and placement of external components preserve the high frequency performance of the OPAx863A devices.** Resistors must be a low reactance type. Surface-mount resistors work best and allow a tighter overall layout. Other network components, such as noninverting input termination resistors, must also be placed close to the package. Keep resistor values as low as possible and consistent with load driving considerations. Lowering the resistor values keep the resistor noise terms low and minimize the effect of its parasitic capacitance; lower resistor values, however, increase the dynamic power consumption because R_F and R_G become part of the amplifiers output load network.

11.2 Layout Example

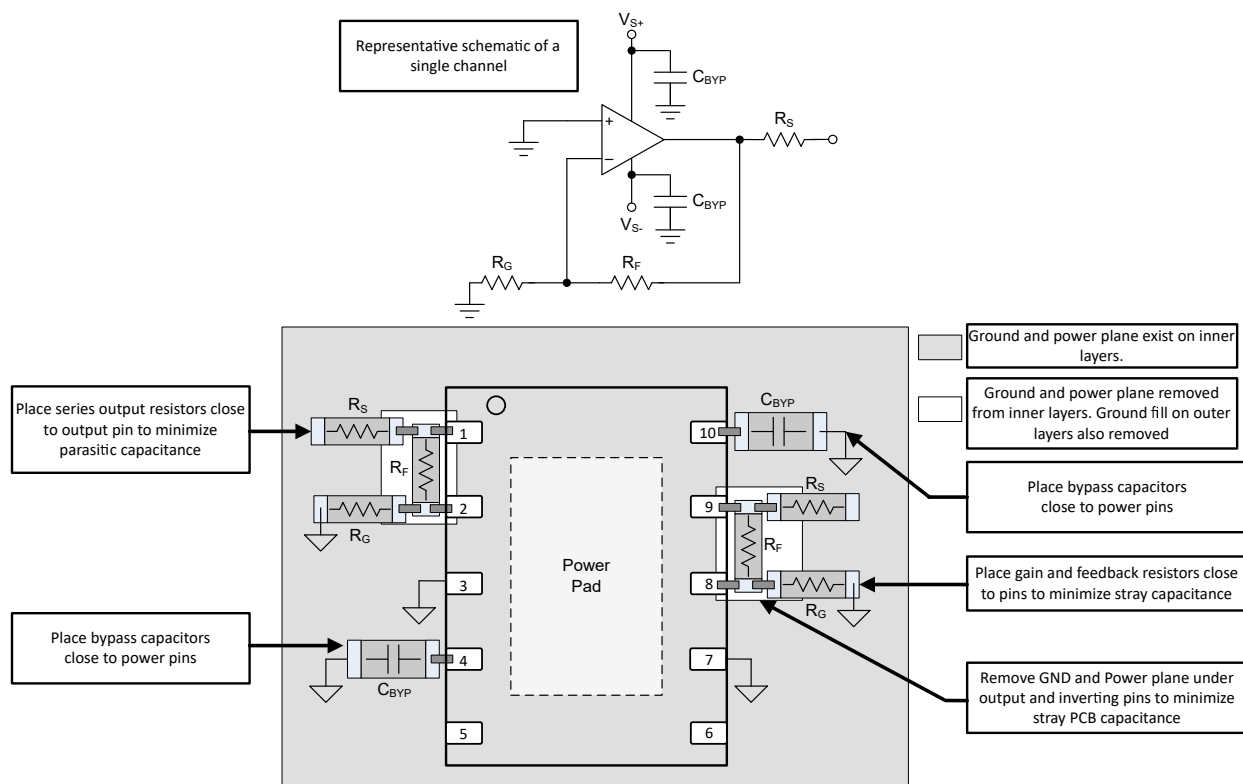


Figure 11-1. Layout Recommendation for Dual-Channel DSN Package

12 Device and Documentation Support

12.1 Documentation Support

12.1.1 Related Documentation

For related documentation, see the following:

- Texas Instruments, [High Speed Amplifiers Generic DSN Evaluation Module user's guide](#)
- Texas Instruments, [Single-Supply Op Amp Design Techniques application report](#)

12.2 Receiving Notification of Documentation Updates

To receive notification of documentation updates, navigate to the device product folder on ti.com. Click on *Subscribe to updates* to register and receive a weekly digest of any product information that has changed. For change details, review the revision history included in any revised document.

12.3 Support Resources

[TI E2E™ support forums](#) are an engineer's go-to source for fast, verified answers and design help — straight from the experts. Search existing answers or ask your own question to get the quick design help you need.

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12.4 Trademarks

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12.5 Electrostatic Discharge Caution



This integrated circuit can be damaged by ESD. Texas Instruments recommends that all integrated circuits be handled with appropriate precautions. Failure to observe proper handling and installation procedures can cause damage.

ESD damage can range from subtle performance degradation to complete device failure. Precision integrated circuits may be more susceptible to damage because very small parametric changes could cause the device not to meet its published specifications.

12.6 Glossary

[TI Glossary](#) This glossary lists and explains terms, acronyms, and definitions.

13 Mechanical, Packaging, and Orderable Information

The following pages include mechanical, packaging, and orderable information. This information is the most current data available for the designated devices. This data is subject to change without notice and revision of this document. For browser-based versions of this data sheet, refer to the left-hand navigation.

PACKAGING INFORMATION

Orderable Device	Status (1)	Package Type	Package Drawing	Pins	Package Qty	Eco Plan (2)	Lead finish/ Ball material (6)	MSL Peak Temp (3)	Op Temp (°C)	Device Marking (4/5)	Samples
OPA2863AIDSNR	ACTIVE	SON	DSN	10	5000	RoHS & Green	NIPDAU	Level-2-260C-1 YEAR	-40 to 125	2863A	Samples

(1) The marketing status values are defined as follows:

ACTIVE: Product device recommended for new designs.

LIFEBUY: TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

NRND: Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

PREVIEW: Device has been announced but is not in production. Samples may or may not be available.

OBsolete: TI has discontinued the production of the device.

(2) **RoHS:** TI defines "RoHS" to mean semiconductor products that are compliant with the current EU RoHS requirements for all 10 RoHS substances, including the requirement that RoHS substance do not exceed 0.1% by weight in homogeneous materials. Where designed to be soldered at high temperatures, "RoHS" products are suitable for use in specified lead-free processes. TI may reference these types of products as "Pb-Free".

RoHS Exempt: TI defines "RoHS Exempt" to mean products that contain lead but are compliant with EU RoHS pursuant to a specific EU RoHS exemption.

Green: TI defines "Green" to mean the content of Chlorine (Cl) and Bromine (Br) based flame retardants meet JS709B low halogen requirements of <=1000ppm threshold. Antimony trioxide based flame retardants must also meet the <=1000ppm threshold requirement.

(3) MSL, Peak Temp. - The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.

(4) There may be additional marking, which relates to the logo, the lot trace code information, or the environmental category on the device.

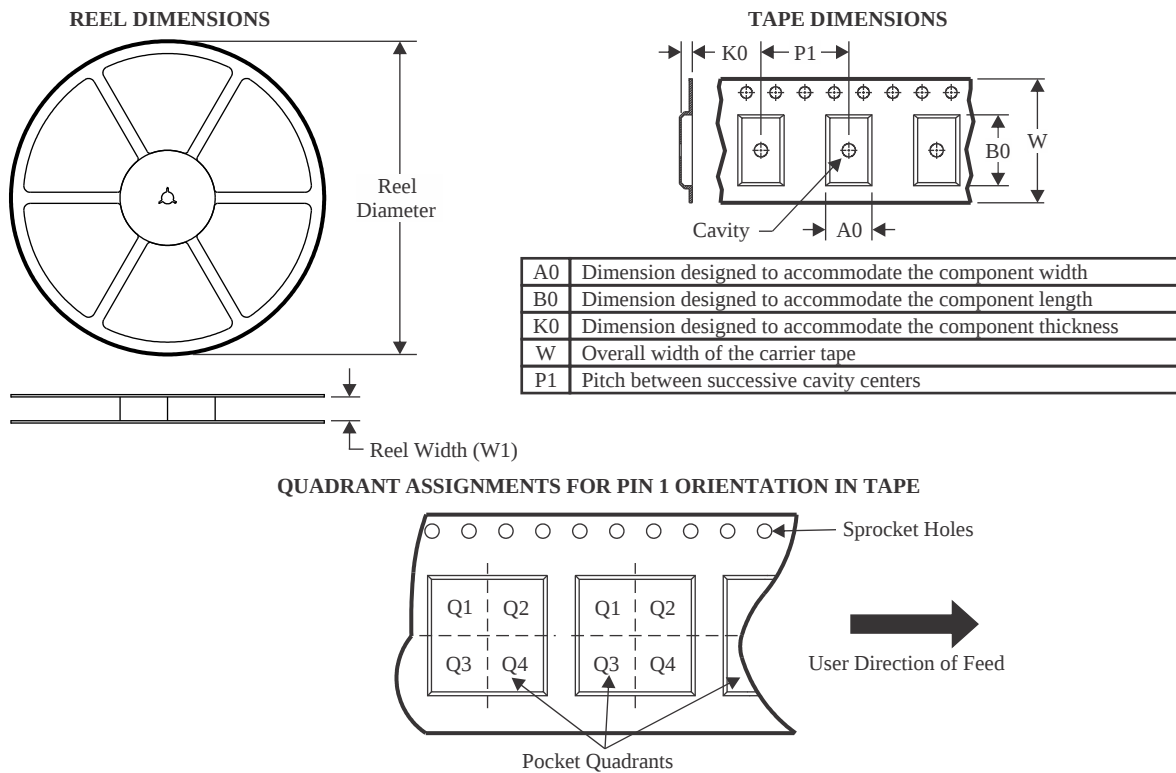
(5) Multiple Device Markings will be inside parentheses. Only one Device Marking contained in parentheses and separated by a "-" will appear on a device. If a line is indented then it is a continuation of the previous line and the two combined represent the entire Device Marking for that device.

(6) Lead finish/Ball material - Orderable Devices may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead finish/Ball material values may wrap to two lines if the finish value exceeds the maximum column width.

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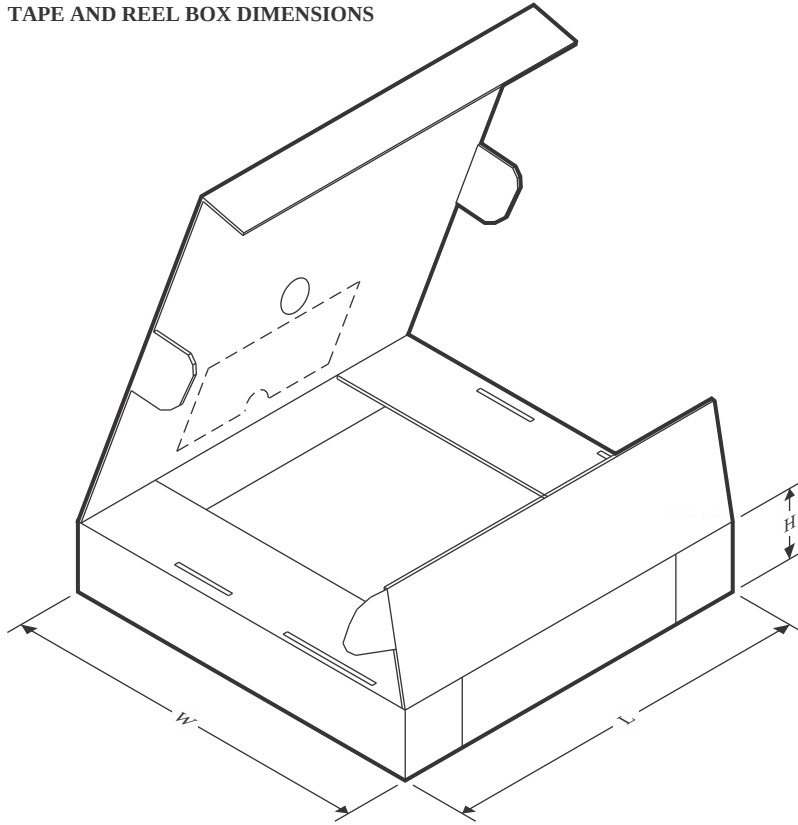
TAPE AND REEL INFORMATION



*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Reel Diameter (mm)	Reel Width W1 (mm)	A0 (mm)	B0 (mm)	K0 (mm)	P1 (mm)	W (mm)	Pin1 Quadrant
OPA2863AIDSNR	SON	DSN	10	5000	330.0	12.4	3.15	3.15	0.75	8.0	12.0	Q2

TAPE AND REEL BOX DIMENSIONS

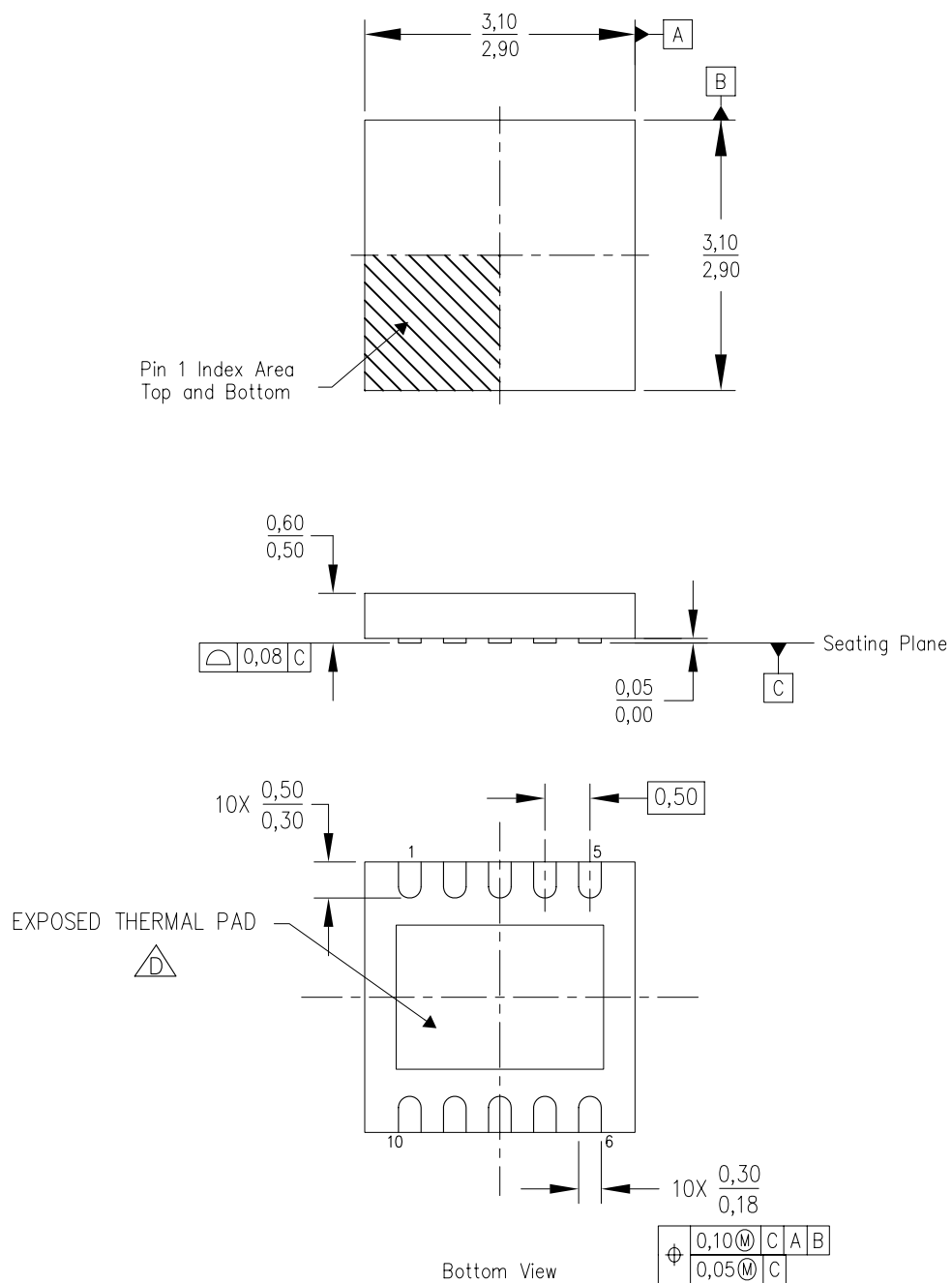


*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Length (mm)	Width (mm)	Height (mm)
OPA2863AIDSNR	SON	DSN	10	5000	364.0	357.0	31.0

DSN (S-PUSON-N10)

PLASTIC QUAD FLATPACK NO-LEAD



4209052/B 11/10

- NOTES:
- A. All linear dimensions are in millimeters. Dimensioning and tolerancing per ASME Y14.5-1994.
 - B. This drawing is subject to change without notice.
 - C. QFN (Quad Flatpack No-Lead) package configuration.
 -  D. The package thermal pad must be soldered to the board for thermal and mechanical performance. See the Product Data Sheet for details regarding the exposed thermal pad dimensions.

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