

# LMC6464QML Quad Micropower, Rail-to-Rail Input and Output CMOS Operational Amplifier

Check for Samples: [LMC6464QML](#)

## FEATURES

- (Typical Unless Otherwise Noted)
- **Low Offset Voltage 500 $\mu$ V**
- **Ultra Low Supply Current 23  $\mu$ A/Amplifier**
- **Operates from 3V to 15V Single Supply**
- **Rail-to-Rail Output Swing**
  - (within 10 mV of Rail,  $V_S = 5V$  and  $R_L = 25 K\Omega$ )
- **Low Input Bias Current 150 fA**

## APPLICATIONS

- **Battery Operated Circuits**
- **Transducer Interface Circuits**
- **Portable Communication Devices**
- **Medical Applications**
- **Battery Monitoring**

## DESCRIPTION

The LMC6464 is a micropower version of the popular LMC6484, combining Rail-to-Rail Input and Output Range with very low power consumption.

The LMC6464 provides an input common-mode voltage range that exceeds both rails. The rail-to-rail output swing of the amplifier, ensured for loads down to 25 K $\Omega$ , assures maximum dynamic signal range. This rail-to-rail performance of the amplifier, combined with its high voltage gain makes it unique among rail-to-rail amplifiers. The LMC6464 is an excellent upgrade for circuits using limited common-mode range amplifiers.

The LMC6464, with ensured specifications at 3V and 5V, is especially well-suited for low voltage applications. A quiescent power consumption of 60  $\mu$ W per amplifier (at  $V_S = 3V$ ) can extend the useful life of battery operated systems. The amplifier's 150 fA input current, low offset voltage of 0.25 mV, and 85 dB CMRR maintain accuracy in battery-powered systems.

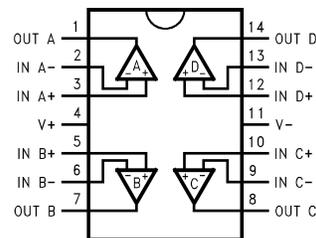


Figure 1. 14-Pin CDIP Top View

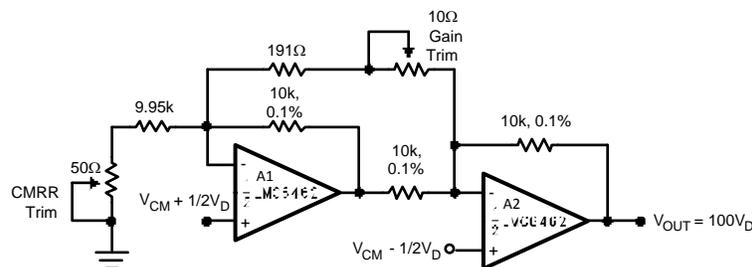


Figure 2. Low-Power Two-Op-Amp Instrumentation Amplifier



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These devices have limited built-in ESD protection. The leads should be shorted together or the device placed in conductive foam during storage or handling to prevent electrostatic damage to the MOS gates.

### Absolute Maximum Ratings <sup>(1)</sup>

Supply Voltage ( $V^+ - V^-$ )			16V
Differential Input Voltage			$\pm$ Supply Voltage
Voltage at Input/Output Pin			$(V^+) + 0.3V, (V^-) - 0.3V$
Current at Input Pin <sup>(2)</sup>			$\pm 5$ mA
Current at Output Pin <sup>(3) (4)</sup>			$\pm 30$ mA
Current at Power Supply Pin			40 mA
Junction Temperature <sup>(3), (5)</sup>			150°C
Power Dissipation <sup>(5)</sup>	LMC6464		6mW
Thermal Resistance <sup>(6)</sup>	$\theta_{JA}$	14LD CDIP (Still Air)	74°C/W
		14LD CDIP (500LF/Min Air flow)	37°C/W
	$\theta_{JC}$	14LD CDIP	8°C/W
Storage Temperature Range			$-65^\circ\text{C} \leq T_A \leq +150^\circ\text{C}$
Lead Temp. (Soldering, 10 sec.)			260°C
ESD Tolerance <sup>(7)</sup>			2.0 kV

- (1) Absolute Maximum Ratings indicate limits beyond which damage to the device may occur. Operating Ratings indicate conditions for which the device is functional, but do not ensure specific performance limits. For ensured specifications and test conditions, see the Electrical Characteristics. The ensured specifications apply only for the test conditions listed. Some performance characteristics may degrade when the device is not operated under the listed test conditions.
- (2) Limiting input pin current is only necessary for input voltages that exceed absolute maximum input voltage ratings.
- (3) Applies to both single supply and split-supply operation. Continuous short circuit operation at elevated ambient temperature can result in exceeding the maximum allowed junction temperature of 150°C. Output currents in excess of  $\pm 30$  mA over long term may adversely affect reliability.
- (4) Do not short circuit output to  $V^+$ , when  $V^+$  is greater than 13V or reliability will be adversely affected.
- (5) The maximum power dissipation must be derated at elevated temperatures and is dictated by  $T_{Jmax}$  (maximum junction temperature),  $\theta_{JA}$  (package junction to ambient thermal resistance), and  $T_A$  (ambient temperature). The maximum allowable power dissipation at any temperature is  $P_{Dmax} = (T_{Jmax} - T_A)/\theta_{JA}$  or the number given in the Absolute Maximum Ratings, whichever is lower.
- (6) All numbers apply for packages soldered directly into a PC board.
- (7) Human body model, 1.5 k $\Omega$  in series with 100 pF.

### Recommended Operating Range <sup>(1)</sup>

Supply Voltage	$3.0V \leq V^+ \leq 15.5V$
Operating Temperature Range	$-55^\circ\text{C} \leq T_A \leq +125^\circ\text{C}$

- (1) Absolute Maximum Ratings indicate limits beyond which damage to the device may occur. Operating Ratings indicate conditions for which the device is functional, but do not ensure specific performance limits. For ensured specifications and test conditions, see the Electrical Characteristics. The ensured specifications apply only for the test conditions listed. Some performance characteristics may degrade when the device is not operated under the listed test conditions.

## Quality Conformance Inspection

Mil-Std-883, Method 5005 - Group A

Subgroup	Description	Temp (°C)
1	Static tests at	+25
2	Static tests at	+125
3	Static tests at	-55
4	Dynamic tests at	+25
5	Dynamic tests at	+125
6	Dynamic tests at	-55
7	Functional tests at	+25
8A	Functional tests at	+125
8B	Functional tests at	-55
9	Switching tests at	+25
10	Switching tests at	+125
11	Switching tests at	-55
12	Settling time at	+25
13	Settling time at	+125
14	Settling time at	-55

## LMC6464 Electrical Characteristics DC Parameters: 3 Volt

 The following conditions apply, unless otherwise specified.  $V^+ = 3V$ ,  $V^- = 0V$ ,  $V_{CM} = V_O = V^+/2$  and  $R_L > 1M$ .

Symbol	Parameter	Conditions	Notes	Min	Max	Units	Sub-groups	
$V_{IO}$	Input Offset Voltage				0.8	mV	1	
					1.7	mV	2	
$I_{IB}$	Input Bias Current		(1)		25	pA	1	
			(1)		100	pA	2	
$I_{IO}$	Input Offset Current		(1)		25	pA	1	
			(1)		100	pA	2, 3	
CMRR	Common Mode Rejection Ratio	$0V \leq V_{CM} \leq 3.0V$			60	dB	1	
					57	dB	2, 3	
$V_{CM}$	Input Common Mode Voltage Range	For CMRR $\geq$ 50 dB			3.0	0.0	V	1
					2.9	0.1	V	2, 3
$V_{Op}$	Output Swing	$R_L = 25K\Omega$ to $V^+/2$			2.9	0.10	V	1
					2.8	0.15	V	2, 3
$I_{CC}$	Supply Current	$V_O = V^+/2$				110	$\mu$ A	1
						140	$\mu$ A	2, 3
$I_{SC}$	Output Short Circuit Current	Sourcing $V_O = 0V$			8.0		mA	1
					6.0		mA	2, 3
		Sinking $V_O = 3V$			23		mA	1
					17		mA	2, 3

(1) Limits are dictated by testing limitations and not device performance.

### LMC6464 Electrical Characteristics DC Parameters: 5 Volt

The following conditions apply, unless otherwise specified.  $V^+ = 5V$ ,  $V^- = 0V$ ,  $V_{CM} = V_O = V^+/2$  and  $R_L > 1M$ .

Symbol	Parameter	Conditions	Notes	Min	Max	Units	Sub-groups	
$V_{IO}$	Input Offset Voltage				0.5	mV	1	
					1.4	mV	2, 3	
$I_{IB}$	Input Bias Current		(1)		25	pA	1	
			(1)		100	pA	2, 3	
$I_{IO}$	Input Offset Current		(1)		25	pA	1	
			(1)		100	pA	2, 3	
CMRR	Common Mode Rejection Ratio	$0V \leq V_{CM} \leq 5.0V$			70	dB	1	
					67	dB	2, 3	
$V_{CM}$	Input Common-Mode Voltage Range	For CMRR $\geq 50$ dB			5.25	-0.10	V	1
					5.00	0.00	V	2, 3
$V_{Op}$	Output Swing	$R_L = 100K\Omega$ to $V^+/2$			4.99	0.01	V	1
					0	0		
		$R_L = 25K\Omega$ to $V^+/2$			4.98	0.02	V	2, 3
					0	0		
$I_{CC}$	Supply Current	$V_O = V^+/2$			110	$\mu$ A	1	
					140	$\mu$ A	2, 3	
$I_{SC}$	Output Short Circuit Current	Sourcing $V_O = 0V$			19	mA	1	
					15	mA	2, 3	
		Sinking $V_O = 5V$			22	mA	1	
					17	mA	2, 3	

(1) Limits are dictated by testing limitations and not device performance.

### LMC6464 Electrical Characteristics DC Parameters: 15 Volt

The following conditions apply, unless otherwise specified.  $V^+ = 15V$ ,  $V^- = 0V$ ,  $V_{CM} = V_O = V^+/2$  and  $R_L > 1M$ .

Symbol	Parameter	Conditions	Notes	Min	Max	Units	Sub-groups	
$V_{IO}$	Input Offset Voltage				1.8	mV	1	
					2.3	mV	2, 3	
$I_{IB}$	Input Bias Current		(1)		25	pA	1	
			(1)		100	pA	2, 3	
$I_{IO}$	Input Offset Current		(1)		25	pA	1	
			(1)		100	pA	2, 3	
CMRR	Common Mode Rejection Ratio	$0V \leq V_{CM} \leq 15.0V$			70	dB	1	
					67	dB	2, 3	
$V_{CM}$	Input Common Mode Voltage Range	For CMRR $\geq 50$ dB			15.25	-0.15	V	1
					15.00	0.00	V	2, 3
+PSRR	Positive Power Supply Rejection Ratio	$5V \leq V^+ \leq 15V$ $V^- = 0V$ , $V_O = 2.5V$			70	dB	1	
					67	dB	2, 3	
-PSRR	Negative Power Supply Rejection Ratio	$-15V \leq V^- \leq -5V$ $V^+ = 0V$ , $V_O = -2.5V$			70	dB	1	
					67	dB	2, 3	

(1) Limits are dictated by testing limitations and not device performance.

**LMC6464 Electrical Characteristics DC Parameters: 15 Volt (continued)**

 The following conditions apply, unless otherwise specified.  $V^+ = 15V$ ,  $V^- = 0V$ ,  $V_{CM} = V_O = V^+/2$  and  $R_L > 1M$ .

Symbol	Parameter	Conditions	Notes	Min	Max	Units	Sub-groups
$V_{Op}$	Output Swing	$R_L = 100K\Omega$ to $V^+/2$		14.975	0.025	V	1
				14.965	0.035	V	2, 3
		$R_L = 25K\Omega$ to $V^+/2$		14.900	0.050	V	1
				14.850	0.150	V	2, 3
$I_{CC}$	Supply Current	$V_O = V^+/2$			120	$\mu A$	1
					140	$\mu A$	2, 3
$I_{SC}$	Output Short Circuit Current	Sourcing $V_O = 0V$		24		mA	1
				17		mA	2, 3
		Sinking $V_O = 12V$	(2)	55		mA	1
			(2)	45		mA	2, 3
$A_V$	Large Signal Voltage Gain	Sourcing $R_L = 100K\Omega$	(3)	110		dB	1
			(3)	80		dB	2, 3
		Sinking $R_L = 100K\Omega$	(3)	100		dB	1
			(3)	70		dB	2, 3
		Sourcing $R_L = 25K\Omega$	(3)	110		dB	1
			(3)	70		dB	2, 3
Sinking $R_L = 25K\Omega$	(3)	95		dB	1		
	(3)	60		dB	2, 3		

 (2) Do not short circuit output to  $V^+$ , when  $V^+$  is greater than 13V or reliability will be adversely affected.

 (3)  $V_{CM} = 7.5V$  and  $R_L$  connected to 7.5V. For Sourcing tests,  $7.5V \leq V_O \leq 11.5V$ . For Sinking tests,  $3.5V \leq V_O \leq 7.5V$ .

**LMC6464 Electrical Characteristics AC Parameters: 15 Volt**

The following conditions apply, unless otherwise specified.

 DC:  $V^+ = 15V$ ,  $V^- = 0V$ ,  $V_{CM} = V_O = V^+/2$  and  $R_L > 1M$ .

Symbol	Parameter	Conditions	Notes	Min	Max	Units	Sub-groups
SR	Slew Rate		(1)	15		V/mS	4
			(1)	7.0		V/mS	5, 6
GBW	Gain-Bandwidth			60		KHz	4
				45		KHz	5, 6

 (1) Device configured as a Voltage Follower with a 10V input step. For positive slew,  $V_I$  swing is 2.5V to 12.5V,  $V_O$  is measured between 6.0V and 9.0V. For negative slew,  $V_I$  swing is 12.5V to 2.5V,  $V_O$  is measured between 9.0V and 6.0V.

### Typical Performance Characteristics

$V_S = +5V$ , Single Supply,  $T_A = 25^\circ C$  unless otherwise specified

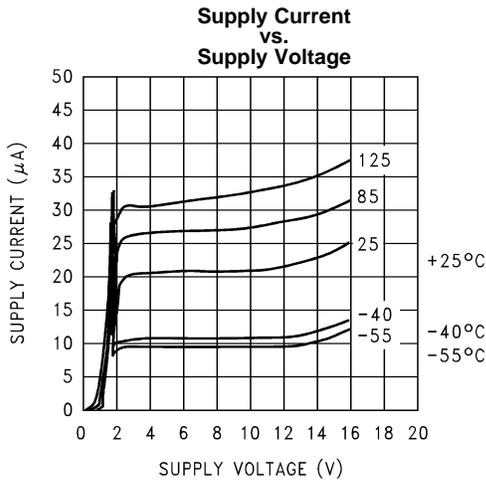


Figure 3.

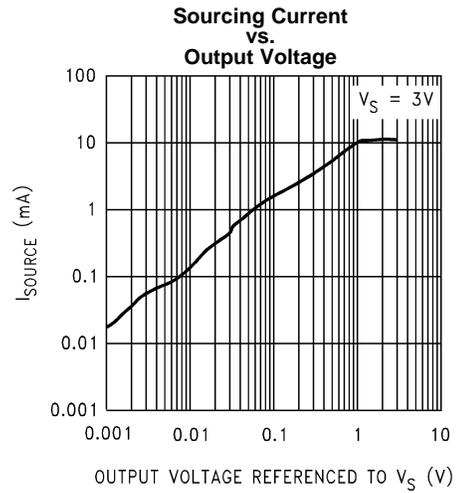


Figure 4.

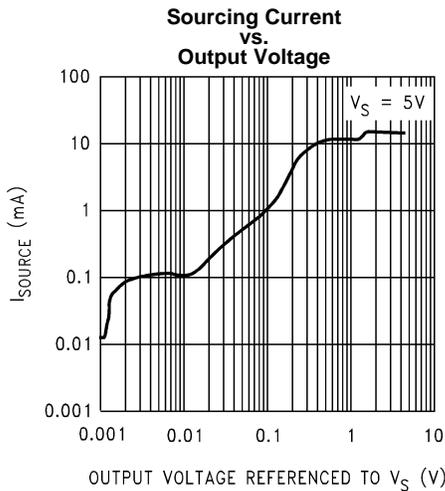


Figure 5.

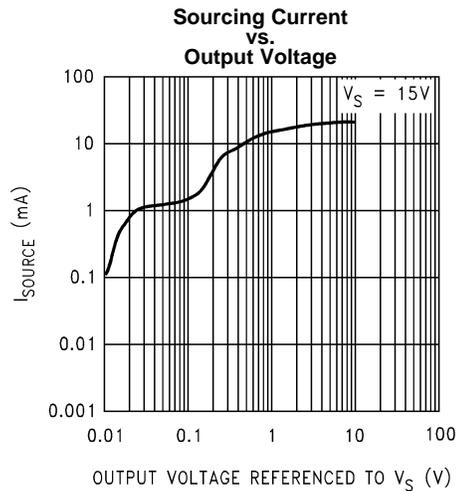


Figure 6.

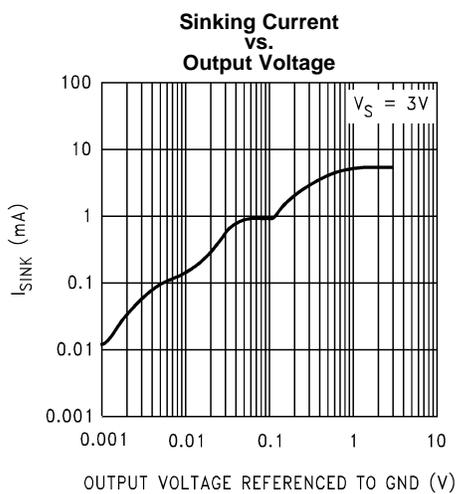


Figure 7.

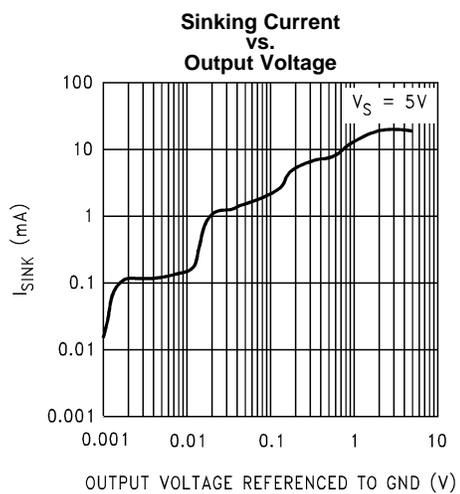


Figure 8.

Typical Performance Characteristics (continued)

$V_S = +5V$ , Single Supply,  $T_A = 25^\circ C$  unless otherwise specified

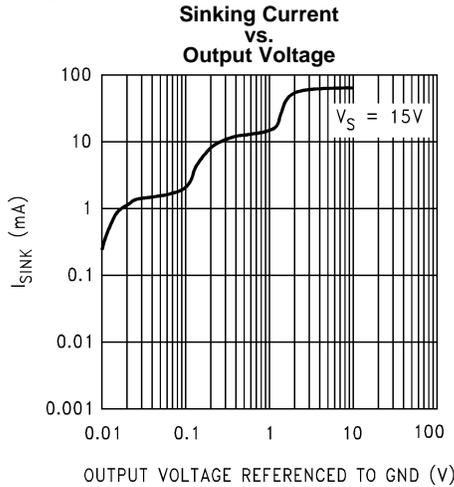


Figure 9.

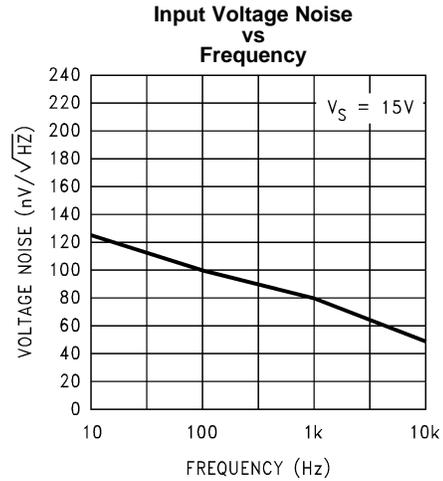


Figure 10.

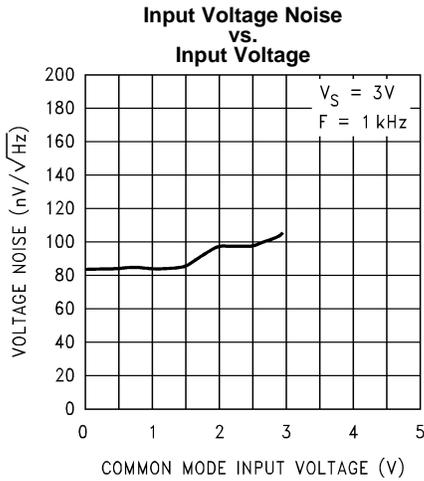


Figure 11.

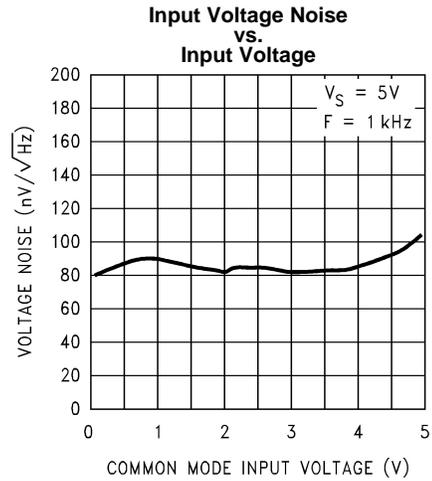


Figure 12.

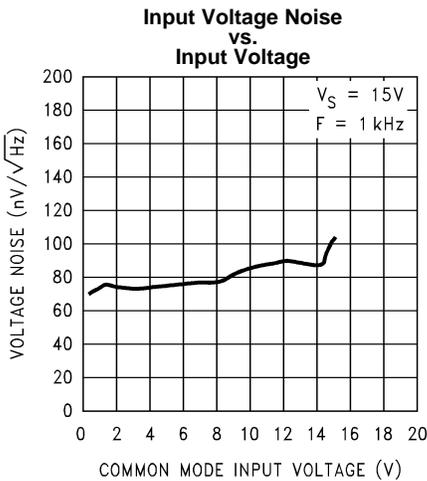


Figure 13.

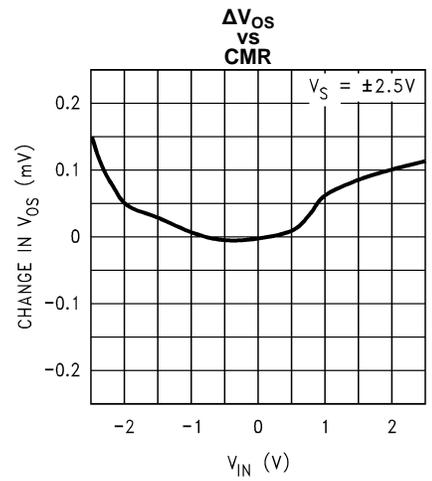
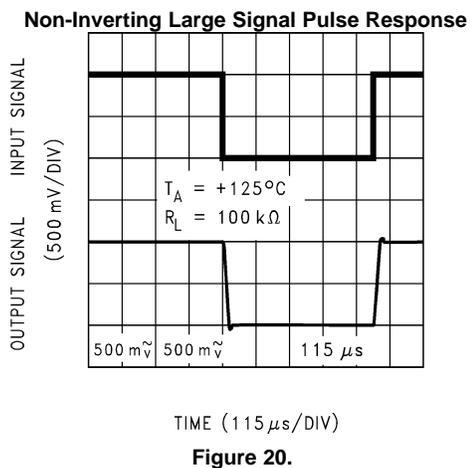
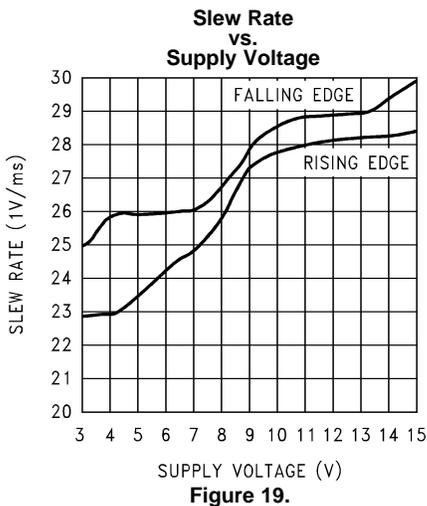
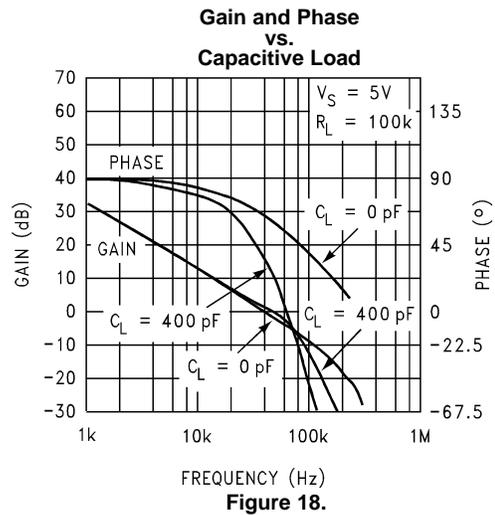
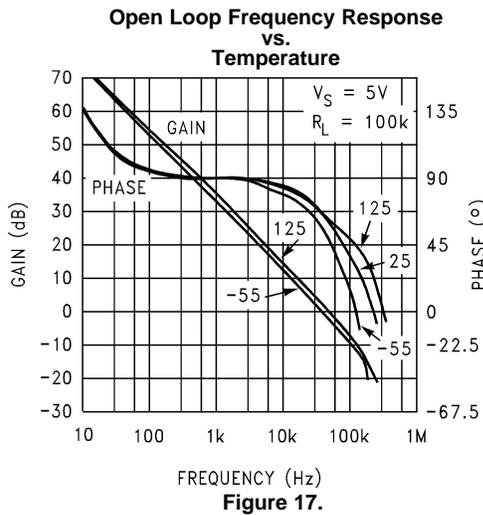
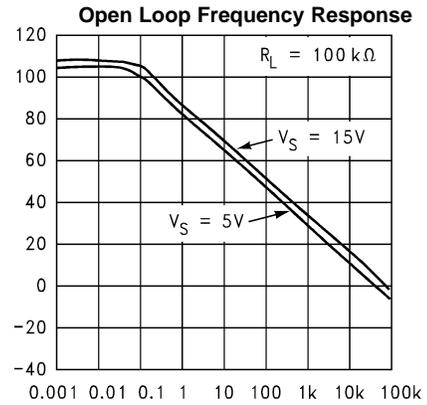
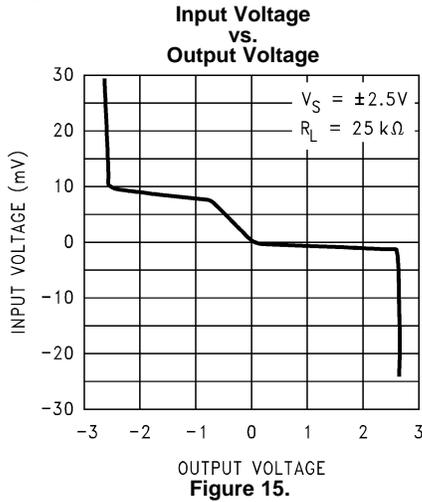


Figure 14.

**Typical Performance Characteristics (continued)**

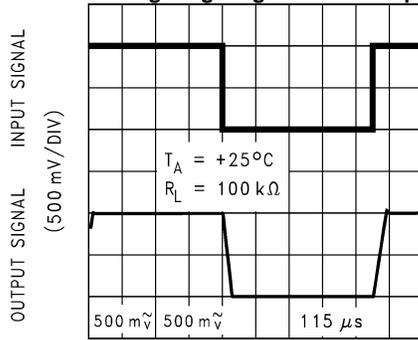
$V_S = +5V$ , Single Supply,  $T_A = 25^\circ C$  unless otherwise specified



Typical Performance Characteristics (continued)

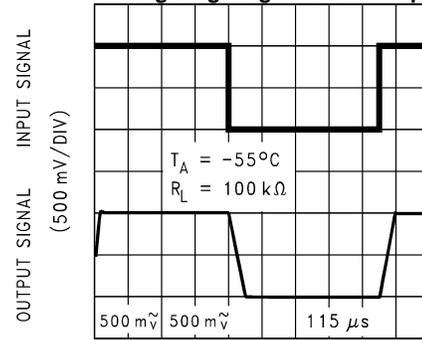
$V_S = +5V$ , Single Supply,  $T_A = 25^\circ C$  unless otherwise specified

Non-Inverting Large Signal Pulse Response



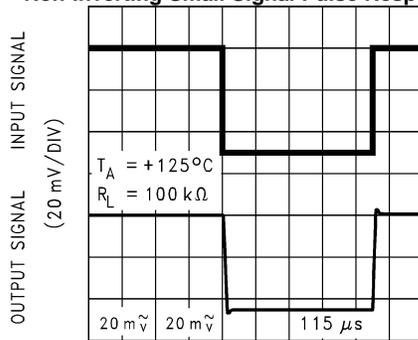
TIME (115  $\mu s$ /DIV)  
Figure 21.

Non-Inverting Large Signal Pulse Response



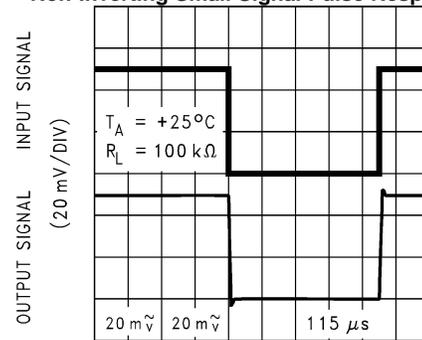
TIME (115  $\mu s$ /DIV)  
Figure 22.

Non-Inverting Small Signal Pulse Response



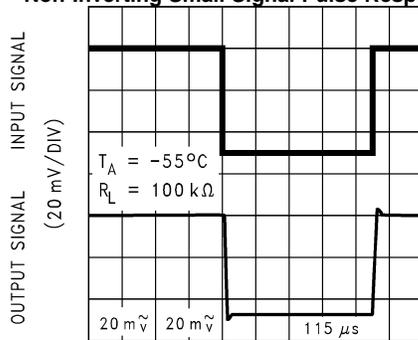
TIME (115  $\mu s$ /DIV)  
Figure 23.

Non-Inverting Small Signal Pulse Response



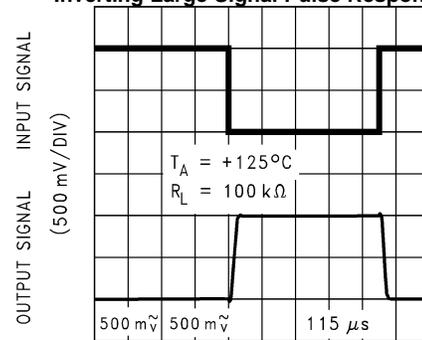
TIME (115  $\mu s$ /DIV)  
Figure 24.

Non-Inverting Small Signal Pulse Response



TIME (115  $\mu s$ /DIV)  
Figure 25.

Inverting Large Signal Pulse Response

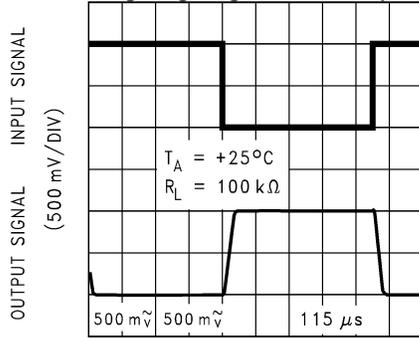


TIME (115  $\mu s$ /DIV)  
Figure 26.

**Typical Performance Characteristics (continued)**

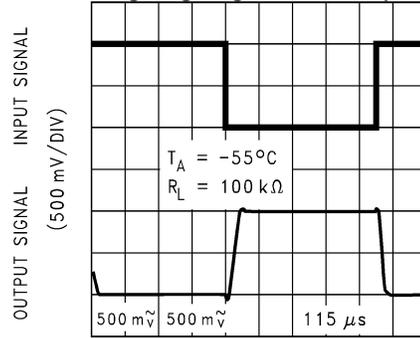
$V_S = +5V$ , Single Supply,  $T_A = 25^\circ C$  unless otherwise specified

**Inverting Large Signal Pulse Response**



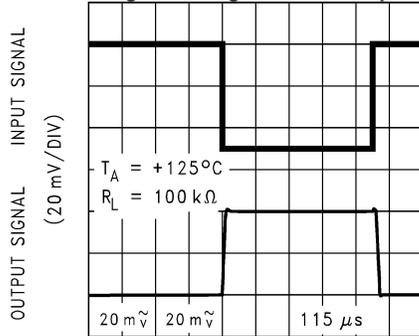
TIME (115  $\mu s$ /DIV)  
**Figure 27.**

**Inverting Large Signal Pulse Response**



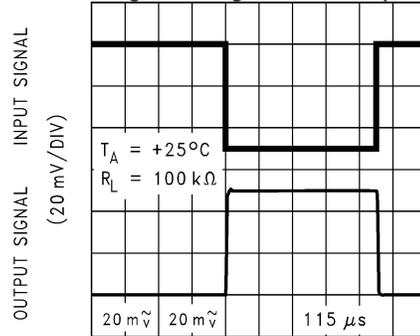
TIME (115  $\mu s$ /DIV)  
**Figure 28.**

**Inverting Small Signal Pulse Response**



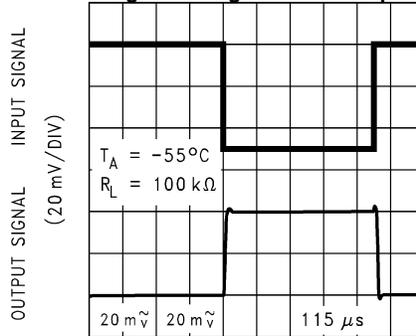
TIME (115  $\mu s$ /DIV)  
**Figure 29.**

**Inverting Small Signal Pulse Response**



TIME (115  $\mu s$ /DIV)  
**Figure 30.**

**Inverting Small Signal Pulse Response**

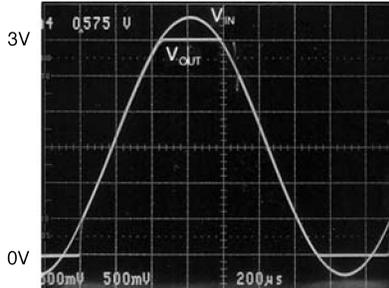


TIME (115  $\mu s$ /DIV)  
**Figure 31.**

## APPLICATION INFORMATION

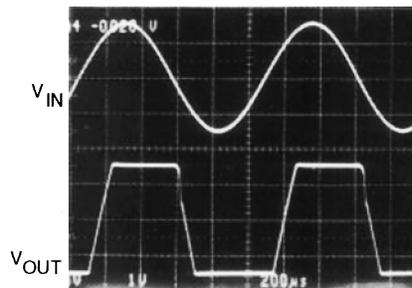
### INPUT COMMON-MODE VOLTAGE RANGE

The LMC6464 has a rail-to-rail input common-mode voltage range. [Figure 32](#) shows an input voltage exceeding both supplies with no resulting phase inversion on the output.

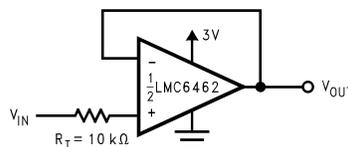


**Figure 32. An Input Voltage Signal Exceeds the LMC6464 Power Supply Voltage with No Output Phase Inversion**

The absolute maximum input voltage at  $V^+ = 3V$  is 300 mV beyond either supply rail at room temperature. Voltages greatly exceeding this absolute maximum rating, as in [Figure 33](#), can cause excessive current to flow in or out of the input pins, possibly affecting reliability. The input current can be externally limited to  $\pm 5$  mA, with an input resistor, as shown in [Figure 34](#).



**Figure 33. A  $\pm 7.5V$  Input Signal Greatly Exceeds the 3V Supply in [Figure 34](#) Causing No Phase Inversion Due to  $R_I$**



**Figure 34. Input Current Protection for Voltages Exceeding the Supply Voltage**

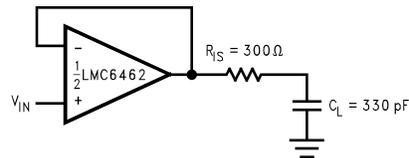
### RAIL-TO-RAIL OUTPUT

The approximated output resistance of the LMC6464 is 180 $\Omega$  sourcing, and 130 $\Omega$  sinking at  $V_S = 3V$ , and 110 $\Omega$  sourcing and 83 $\Omega$  sinking at  $V_S = 5V$ . The maximum output swing can be estimated as a function of load using the calculated output resistance.

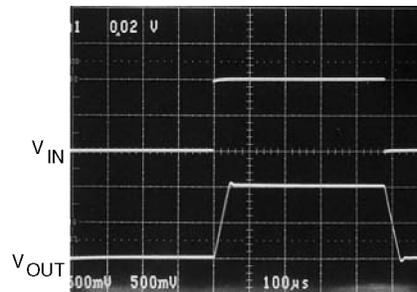
## CAPACITIVE LOAD TOLERANCE

The LMC6464 can typically drive a 200 pF load with  $V_S = 5V$  at unity gain without oscillating. The unity gain follower is the most sensitive configuration to capacitive load. Direct capacitive loading reduces the phase margin of op-amps. The combination of the op-amp's output impedance and the capacitive load induces phase lag. This results in either an underdamped pulse response or oscillation.

Capacitive load compensation can be accomplished using resistive isolation as shown in [Figure 35](#). If there is a resistive component of the load in parallel to the capacitive component, the isolation resistor and the resistive load create a voltage divider at the output. This introduces a DC error at the output.



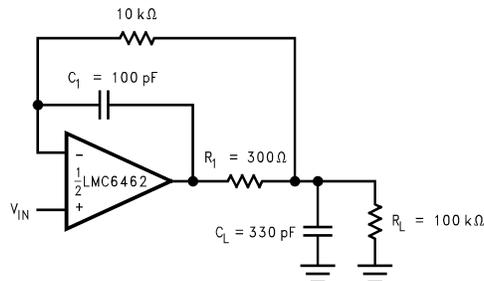
**Figure 35. Resistive Isolation of a 300 pF Capacitive Load**



**Figure 36. Pulse Response of the LMC6464 Circuit Shown in [Figure 35](#)**

[Figure 36](#) displays the pulse response of the LMC6464 circuit in [Figure 35](#).

Another circuit, shown in [Figure 37](#), is also used to indirectly drive capacitive loads. This circuit is an improvement to the circuit shown in [Figure 35](#) because it provides DC accuracy as well as AC stability. R1 and C1 serve to counteract the loss of phase margin by feeding the high frequency component of the output signal back to the amplifiers inverting input, thereby preserving phase margin in the overall feedback loop. The values of R1 and C1 should be experimentally determined by the system designer for the desired pulse response. Increased capacitive drive is possible by increasing the value of the capacitor in the feedback loop.



**Figure 37. LMC6464 Non-Inverting Amplifier, Compensated to Handle a 300 pF Capacitive and 100 KΩ Resistive Load**

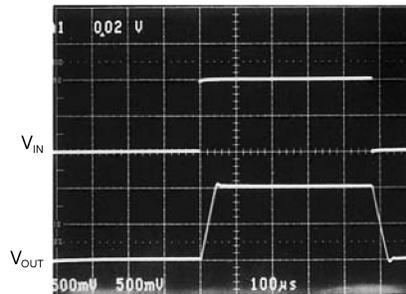


Figure 38. Pulse Response of LMC6464 Circuit in Figure 37

The pulse response of the circuit shown in Figure 37 is shown in Figure 38.

### COMPENSATING FOR INPUT CAPACITANCE

It is quite common to use large values of feedback resistance with amplifiers that have ultra-low input current, like the LMC6464. Large feedback resistors can react with small values of input capacitance due to transducers, photodiodes, and circuits board parasitics to reduce phase margins.

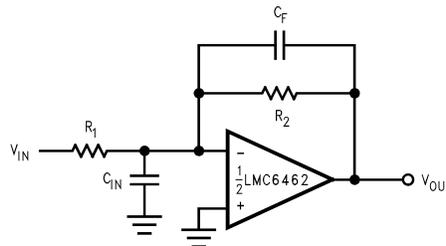


Figure 39. Canceling the Effect of Input Capacitance

The effect of input capacitance can be compensated for by adding a feedback capacitor. The feedback capacitor (as in Figure 39),  $C_F$ , is first estimated by:

$$\frac{1}{2\pi R_1 C_{IN}} \geq \frac{1}{2\pi R_2 C_F} \quad (1)$$

or

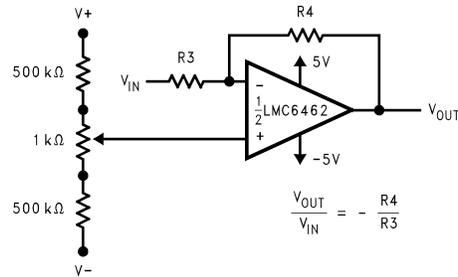
$$R_1 C_1 \leq R_2 C_F \quad (2)$$

which typically provides significant overcompensation.

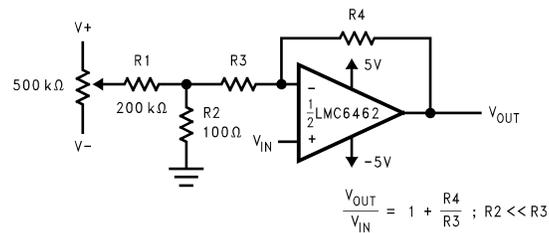
Printed circuit board stray capacitance may be larger or smaller than that of a breadboard, so the actual optimum value for  $C_F$  may be different. The values of  $C_F$  should be checked on the actual circuit. (Refer to the LMC660 quad CMOS amplifier data sheet for a more detailed discussion.)

### OFFSET VOLTAGE ADJUSTMENT

Offset voltage adjustment circuits are illustrated in Figure 40 and Figure 41. Large value resistances and potentiometers are used to reduce power consumption while providing typically  $\pm 2.5$  mV of adjustment range, referred to the input, for both configurations with  $V_S = \pm 5V$ .



**Figure 40. Inverting Configuration, Offset Voltage Adjustment**



**Figure 41. Non-Inverting Configuration, Offset Voltage Adjustment**

## SPICE MACROMODEL

A Spice macromodel is available for the LMC6464. This model includes a simulation of:

- Input common-mode voltage range
- Frequency and transient response
- GBW dependence on loading conditions
- Quiescent and dynamic supply current
- Output swing dependence on loading conditions

and many more characteristics as listed on the macromodel disk.

Contact the Texas Instruments Customer Response Center to obtain an operational amplifier Spice model library disk.

## PRINTED-CIRCUIT-BOARD LAYOUT FOR HIGH-IMPEDANCE WORK

It is generally recognized that any circuit which must operate with less than 1000 pA of leakage current requires special layout of the PC board. When one wishes to take advantage of the ultra-low input current of the LMC6464, typically 150 fA, it is essential to have an excellent layout. Fortunately, the techniques of obtaining low leakages are quite simple. First, the user must not ignore the surface leakage of the PC board, even though it may sometimes appear acceptably low, because under conditions of high humidity or dust or contamination, the surface leakage will be appreciable.

To minimize the effect of any surface leakage, lay out a ring of foil completely surrounding the LMC6464's inputs and the terminals of capacitors, diodes, conductors, resistors, relay terminals, etc. connected to the op-amp's inputs, as in [Figure 42](#). To have a significant effect, guard rings should be placed in both the top and bottom of the PC board. This PC foil must then be connected to a voltage which is at the same voltage as the amplifier inputs, since no leakage current can flow between two points at the same potential. For example, a PC board trace-to-pad resistance of  $10^{12}\Omega$ , which is normally considered a very large resistance, could leak 5 pA if the trace were a 5V bus adjacent to the pad of the input. This would cause a 30 times degradation from the LMC6464's actual performance. However, if a guard ring is held within 5 mV of the inputs, then even a resistance of  $10^{11}\Omega$  would cause only 0.05 pA of leakage current. See [Typical Connections of Guard Rings](#) for standard op-amp configurations.

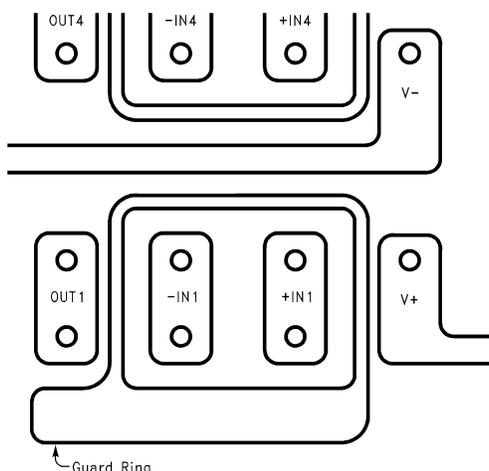


Figure 42. Example of Guard Ring in P.C. Board Layout

### Typical Connections of Guard Rings

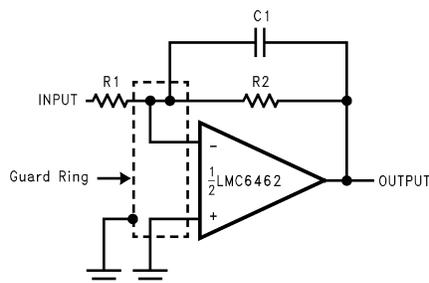


Figure 43. Inverting Amplifier

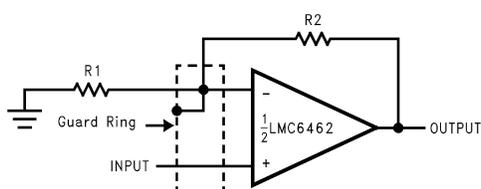


Figure 44. Non-Inverting Amplifier

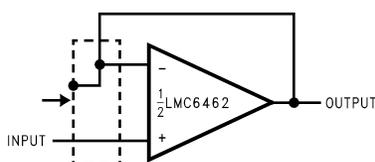
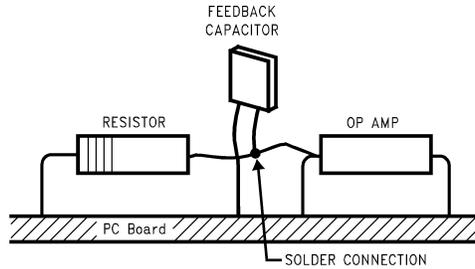


Figure 45. Follower

The designer should be aware that when it is inappropriate to lay out a PC board for the sake of just a few circuits, there is another technique which is even better than a guard ring on a PC board: Don't insert the amplifier's input pin into the board at all, but bend it up in the air and use only air as an insulator. Air is an excellent insulator. In this case you may have to forego some of the advantages of PC board construction, but the advantages are sometimes well worth the effort of using point-to-point up-in-the-air wiring. See [Figure 46](#).



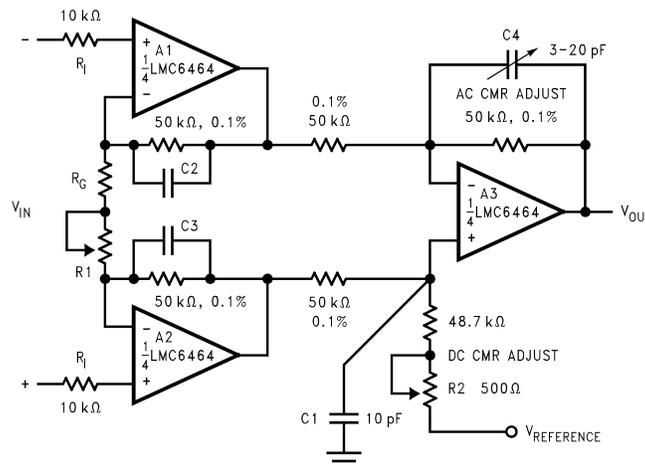
(Input pins are lifted out of PC board and soldered directly to components. All other pins connected to PC board.)

**Figure 46. Air Wiring**

**INSTRUMENTATION CIRCUITS**

The LMC6464 has the high input impedance, large common-mode range and high CMRR needed for designing instrumentation circuits. Instrumentation circuits designed with the LMC6464 can reject a larger range of common-mode signals than most in-amps. This makes instrumentation circuits designed with the LMC6464 an excellent choice for noisy or industrial environments. Other applications that benefit from these features include analytic medical instruments, magnetic field detectors, gas detectors, and silicon-based transducers.

A small valued potentiometer is used in series with  $R_G$  to set the differential gain of the three op-amp instrumentation circuit in Figure 47. This combination is used instead of one large valued potentiometer to increase gain trim accuracy and reduce error due to vibration.



**Figure 47. Low Power Three Op-Amp Instrumentation Amplifier**

A two op-amp instrumentation amplifier designed for a gain of 100 is shown in Figure 48. Low sensitivity trimming is made for offset voltage, CMRR and gain. Low cost and low power consumption are the main advantages of this two op-amp circuit.

Higher frequency and larger common-mode range applications are best facilitated by a three op-amp instrumentation amplifier.

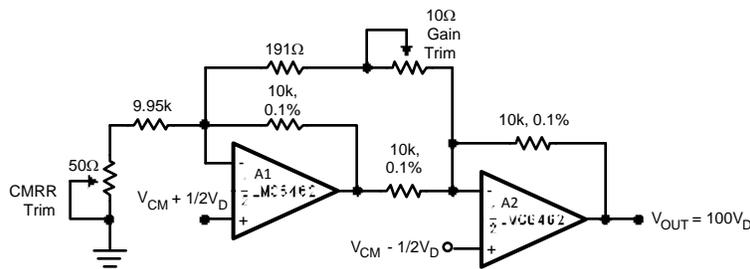


Figure 48. Low-Power Two-Op-Amp Instrumentation Amplifier

## Typical Single-Supply Applications

### TRANSDUCER INTERFACE CIRCUITS

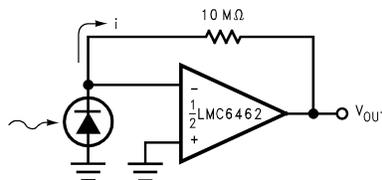


Figure 49. Photo Detector Circuit

Photocells can be used in portable light measuring instruments. The LMC6464, which can be operated off a battery, is an excellent choice for this circuit because of its very low input current and offset voltage.

### LMC6464 AS A COMPARATOR

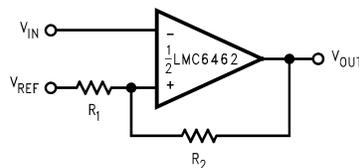


Figure 50. Comparator with Hysteresis

Figure 50 shows the application of the LMC6464 as a comparator. The hysteresis is determined by the ratio of the two resistors. The LMC6464 can thus be used as a micropower comparator, in applications where the quiescent current is an important parameter.

### HALF-WAVE AND FULL-WAVE RECTIFIERS

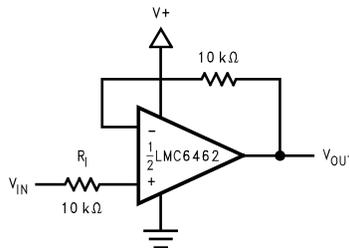
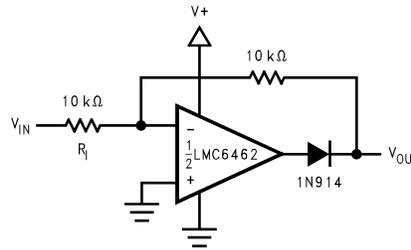


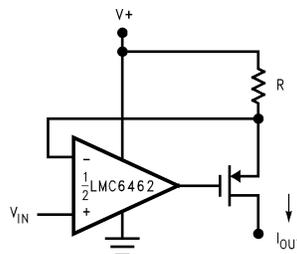
Figure 51. Half-Wave Rectifier with Input Current Protection ( $R_1$ )



**Figure 52. Full-Wave Rectifier with Input Current Protection (R<sub>1</sub>)**

In [Figure 51](#) [Figure 52](#), R<sub>1</sub> limits current into the amplifier since excess current can be caused by the input voltage exceeding the supply voltage.

**PRECISION CURRENT SOURCE**

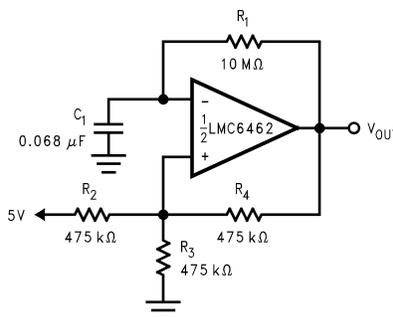


**Figure 53. Precision Current Source**

The output current I<sub>OUT</sub> is given by:

$$I_{OUT} = \left( \frac{V^+ - V_{IN}}{R} \right) \tag{3}$$

**OSCILLATORS**



**Figure 54. 1 Hz Square-Wave Oscillator**

For single supply 5V operation, the output of the circuit will swing from 0V to 5V. The voltage divider set up R<sub>2</sub>, R<sub>3</sub> and R<sub>4</sub> will cause the non-inverting input of the LMC6464 to move from 1.67V (1/3 of 5V) to 3.33V (2/3 of 5V). This voltage behaves as the threshold voltage.

R<sub>1</sub> and C<sub>1</sub> determine the time constant of the circuit. The frequency of oscillation, f<sub>OSC</sub> is

$$\left( \frac{1}{2\Delta t} \right) \tag{4}$$

where Δt is the time the amplifier input takes to move from 1.67V to 3.33V. The calculations are shown below.

$$1.67 = 5 \left( 1 - e^{-\frac{t_1}{\tau}} \right) \quad (5)$$

where  $\tau = RC = 0.68$  seconds

$\rightarrow t_1 = 0.27$  seconds.

and

$$3.33 = 5 \left( 1 - e^{-\frac{t_2}{\tau}} \right) \quad (6)$$

$\rightarrow t_2 = 0.75$  seconds

Then,

$$f_{\text{OSC}} = \left( \frac{1}{2\Delta t} \right) \quad (7)$$

$$= \frac{1}{2(0.75 - 0.27)} \quad (8)$$

= 1 Hz

### LOW FREQUENCY NULL

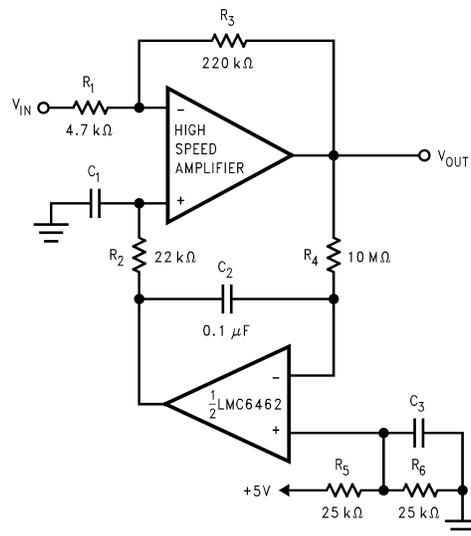


Figure 55. High Gain Amplifier with Low Frequency Null

Output offset voltage is the error introduced in the output voltage due to the inherent input offset voltage  $V_{OS}$ , of an amplifier.

Output Offset Voltage = (Input Offset Voltage) (Gain)

In the above configuration, the resistors  $R_5$  and  $R_6$  determine the nominal voltage around which the input signal,  $V_I$  should be symmetrical. The high frequency component of the input signal  $V_I$  will be unaffected while the low frequency component will be nulled since the DC level of the output will be the input offset voltage of the LMC6464 plus the bias voltage. This implies that the output offset voltage due to the top amplifier will be eliminated.

**Table 1. Revision History**

Released	Revision	Section	Changes
12/08/2010	A	New Release, Corporate format	1 MDS data sheets converted into one Corp. data sheet format. MNLMC6464AM-X Rev 1A1 will be archived.
03/26/2013	A	All	Changed layout of National Data Sheet to TI format.

**PACKAGING INFORMATION**

Orderable Device	Status (1)	Package Type	Package Drawing	Pins	Package Qty	Eco Plan (2)	Lead/Ball Finish	MSL Peak Temp (3)	Op Temp (°C)	Top-Side Markings (4)	Samples
5962-9560302QCA	ACTIVE	CDIP	J	14	25	TBD	Call TI	Call TI	-55 to 125	LMC6464AMJ-QML 5962-9560302QCA Q	<a href="#">Samples</a>
LMC6464AMJ-QML	ACTIVE	CDIP	J	14	25	TBD	Call TI	Call TI	-55 to 125	LMC6464AMJ-QML 5962-9560302QCA Q	<a href="#">Samples</a>

(1) The marketing status values are defined as follows:

**ACTIVE:** Product device recommended for new designs.

**LIFEBUY:** TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

**NRND:** Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

**PREVIEW:** Device has been announced but is not in production. Samples may or may not be available.

**OBSOLETE:** TI has discontinued the production of the device.

(2) Eco Plan - The planned eco-friendly classification: Pb-Free (RoHS), Pb-Free (RoHS Exempt), or Green (RoHS & no Sb/Br) - please check <http://www.ti.com/productcontent> for the latest availability information and additional product content details.

**TBD:** The Pb-Free/Green conversion plan has not been defined.

**Pb-Free (RoHS):** TI's terms "Lead-Free" or "Pb-Free" mean semiconductor products that are compatible with the current RoHS requirements for all 6 substances, including the requirement that lead not exceed 0.1% by weight in homogeneous materials. Where designed to be soldered at high temperatures, TI Pb-Free products are suitable for use in specified lead-free processes.

**Pb-Free (RoHS Exempt):** This component has a RoHS exemption for either 1) lead-based flip-chip solder bumps used between the die and package, or 2) lead-based die adhesive used between the die and leadframe. The component is otherwise considered Pb-Free (RoHS compatible) as defined above.

**Green (RoHS & no Sb/Br):** TI defines "Green" to mean Pb-Free (RoHS compatible), and free of Bromine (Br) and Antimony (Sb) based flame retardants (Br or Sb do not exceed 0.1% by weight in homogeneous material)

(3) MSL, Peak Temp. -- The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.

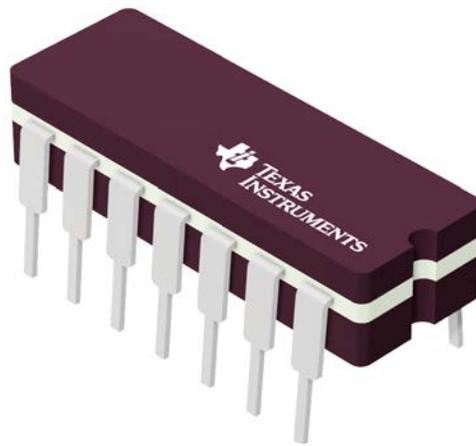
(4) Multiple Top-Side Markings will be inside parentheses. Only one Top-Side Marking contained in parentheses and separated by a "~" will appear on a device. If a line is indented then it is a continuation of the previous line and the two combined represent the entire Top-Side Marking for that device.

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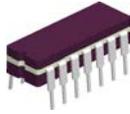
**GENERIC PACKAGE VIEW**  
**CDIP - 5.08 mm max height**  
CERAMIC DUAL IN LINE PACKAGE



Images above are just a representation of the package family, actual package may vary.  
Refer to the product data sheet for package details.

4040083-5/G

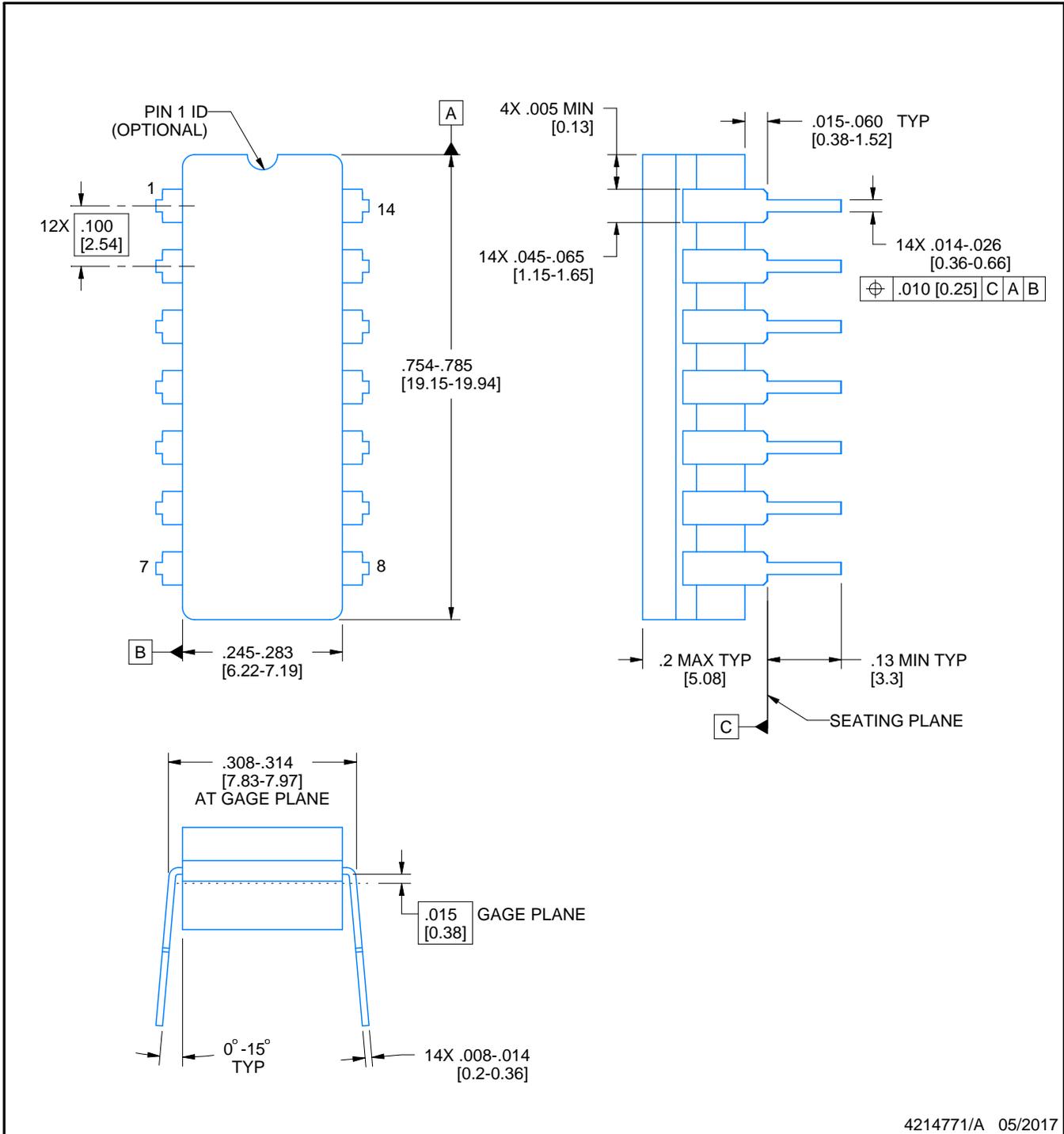
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# PACKAGE OUTLINE

CDIP - 5.08 mm max height

CERAMIC DUAL IN LINE PACKAGE



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NOTES:

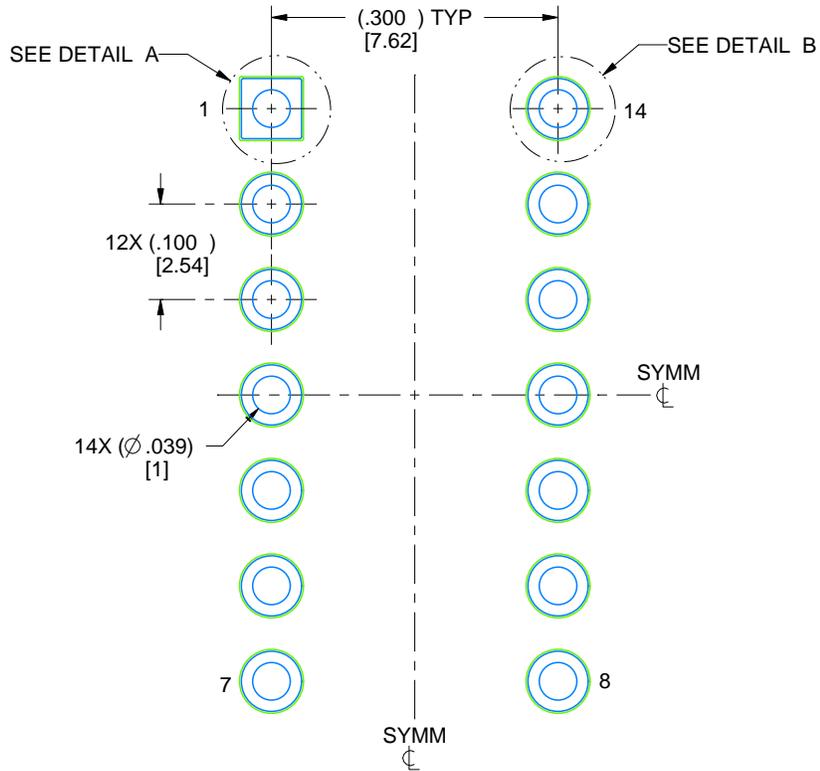
1. All controlling linear dimensions are in inches. Dimensions in brackets are in millimeters. Any dimension in brackets or parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M.
2. This drawing is subject to change without notice.
3. This package is hermetically sealed with a ceramic lid using glass frit.
4. Index point is provided on cap for terminal identification only and on press ceramic glass frit seal only.
5. Falls within MIL-STD-1835 and GDIP1-T14.

# EXAMPLE BOARD LAYOUT

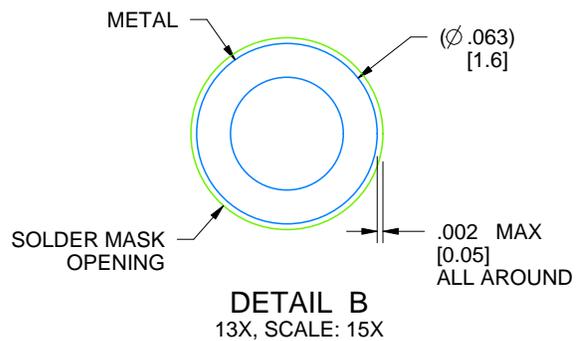
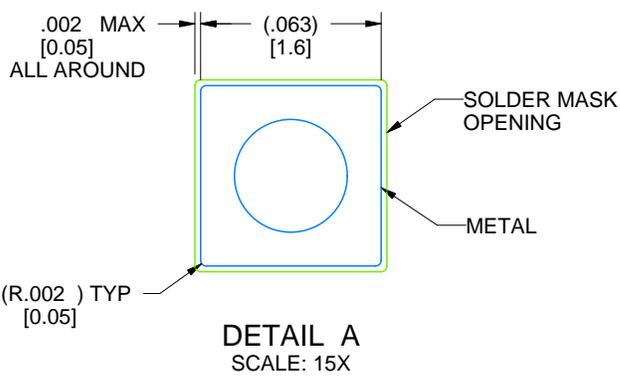
J0014A

CDIP - 5.08 mm max height

CERAMIC DUAL IN LINE PACKAGE



LAND PATTERN EXAMPLE  
NON-SOLDER MASK DEFINED  
SCALE: 5X



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